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ATMOSPHERIC MARINE BOUNDARY LAYER MIXING RATES IN THE CALIFORNIA COASTAL REGION

G. E. Schacher and K. L. Davidson Environmental Physics Group C. W. Fairall, BDM Corporation Naval Postgraduate School Monterey, California

May 1980

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Prepared for: California Air Resources Board 1709 11th Street Sacramento, CA 95814

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The work reported herein was supported in part by the California Air Resources Board, Sacramento, California.

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SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)				
REPORT DOCUMENTATION PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM			
	3. RECIPIENT'S CATALOG NUMBER 5.10 +			
. TITLE (AND SUBTRILE)	5. TYPE OF REPORT & PERIOD COVERED			
ATMOSPHERIC MARINE BOUNDARY LAYER MIXING BATES IN THE CALIFORNIA COASTAL REGION	Technical Report			
	6. PERFORMING ORG. REPORT NUMBER			
7. AUTHOR(a)	8. CONTRACT OR GRANT NUMBER(s)			
G.E. Schacher, C.W. Fairall K.L. Davidson				
9. PERFORMING ORGANISATION NAME AND ADDRESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS			
9 Technical reptos?				
11. CONTROLLING OFFICE NAME AND ADDRESS California Air Resources Board	12. REPORT DATE			
1709 11th St.	13. NUMBER OF PAGES			
Sacramento, CA 95814 14. MONITORING AGENCY NAME & ADDRESS(II dillerent from Controlling Office)	18. SECURITY CLASS. (of this report)			
	Unclassified			
	15a. DECLASSIFICATION/DOWNGRADING			
	SCHEDULE			
Approved for public release; distribution unlimited				
18. SUPPLEMENTARY NOTES	······································			
19. KEY WORDS (Continue on reverse side if necessary and identity by block number)				
Marine Boundary Layer, Mixing Rate, Air Pollution				
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The Naval Postgraduate School has conducted five research cruises in California coastal waters for which sufficient data was obtained to allow boundary layer mixing rates to be determined. These data have been processed to determine the mixing rates. The rates have been correlated with meteorological conditions and geographical location and average values for use in air pollution models have been determined. A simplified method for calculating the mixing rate from mean meteorological parameters is presented.

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I. Introduction

The rate at which air is mixed throughout the atmospheric boundary layer is one of the determinating factors in air quality. The mixing rate governs how rapidly pollutants from surface sources are transported upward, and thus is one of the factors that determines peak concentration in a given volume. Air pollution models divide a particular air shed area into numerous sections (cells) then solve for temporal variations of pollutant density within each cell using source strength and diffusion within the cell and flux across the cell boundaries as input parameters. Matching conditions at the boundaries leads to an overall solution to the problem. The transport across cell boundaries depends mainly on mean wind speed. The transport out of the top of a cell and vertical dispersion within a cell are due to turbulent mixing.

Many of the model cells are over the water for air sheds along the California coast. In the past, there has been little data available that would allow over ocean mixing rates to be determined so estimates of the rate have been based on overland values. The purpose of the work reported here is to determine the needed mixing rates from available Naval Postgraduate School (NPS) data.

The environmental Physics Group of NPS has conducted several research cruises over the past five years in both the Atlantic and East Pacific, at all times of the year, so that a considerable data base has been developed for a wide range of marine atmospheric conditions. Five of these cruises were conducted in

California coastal waters and the data needed to determine boundary layer mixing rates were collected.

These data have been gathered near enough to the coast to be representative of overwater cells in current air pollution models, and far enough at sea so that open ocean conditions prevail. The immediate areas of the three most populous centers, San Francisco, Los Angeles, and San Diego have been extensively investigated. A wide range of meteorological conditions have been encountered, and operations were carried out around the clock. Thus, the available data base allows determinations of mixing rates and their dependence on location and conditions including diurnal variations. In general, conditions over the water do not vary nearly as much as overland. In California coastal waters conditions are generally unstable with slightly stable encountered occasionally.

II. Instrumentation

The studies of California coastal waters have all been carried out aboard the NPS ship R/V ACANIA, which is equipped to make multilevel mean and fluctuation measurements. Available sensor heights above mean sea level are 1, 4, 7, 14.5, 20.5 meters. For most of the data reported here, 4.2, 7.0, and 20.5 meters were used. Boundary layer properties were determined by three techniques:

- 1. bulk aerodynamic (air-sea differences)
- 2. inertial subrange turbulence
- 3. mean profiles

Rather than list all of the shipboard equipment here, we restrict the description to that which is pertinent to determining mixing rates. The measurements needed and the equipment used were:

Sea surface temperature (T_S)

Air temperature (Ta)

Humidity/Dew Point (TD)

Relative wind speed and direction (U)

Temperature inversion height (Z_1)

Wind speed fluctuation (U')

Air temperature fluctuation (T')

- T_s : 1) Hewlett Packard 2801A quartz thermometer (0.1°C)
 - 2) Barnes PRT-5 infrared thermometer (0.3°C)

The HP sensor is floated and averages to about six inches below the surface.

- Ta: Same Hewlett Packard System (±0.2°C)

 Sensors installed in RM Young Gill aspirators.

 The lower opening of the aspirator has been fitted with a radiation shield which improves its performance.
- T_D : General Eastern 1200 AP (T_D , ± 0.3 °C)

 Dew point measured by cooled mirror technique
- U: MRI 1022 (±0.5 knt, ±10°)
 The cups are low threshold so that 1 knt can be measured. Due to inaccuracies in ship speed true wind error is +1 knt, +15° at best.
- Z₁: Aerovironment Model 200 acoustic sounder (±20m)
 Enclosure designed for shipboard allows good
 signal to noise when ship is in motion.
- U': TSI 1054B Hot Wire Anemometer Sensor is 1210 probe mounted with platinum film on quartz cylinder (60 μ) substrate.
- T': Sylvania 140 Thermosonde $Sensor \ \mbox{is TSI 1210 probe mounted with 2.5} \ \mu$ platinum wire.

The equipment evolved with time and the equipment described above is the latest version used.

Sensors were mounted on the R/V ACANIA so that the ship disturbs the sampled air as little as possible. The sensors at 1 m height are placed on a bouy foreward of the ships bow (data

from this height is not used here). The 4 m and 7 m sensors were mounted forward of the ship on a mast placed directly on the bow. The 14.5 m level suffers the most ship influence and this data was only used under special circumstances. The 14.5 m and 20.5 m levels were located on a mast aproximately 15 ft. behind the bow. We attempt to obtain data only when the relative wind is within 30° of the bow but this is not always possible. Even with the precautions of best sensor placement and good relative wind direction it has not been possible to obtain reliable wind profiles on the ship.

Several methods of signal processing and data acquisition were used. This gives as much flexiblity as possible in choosing which of the three methods is used in the computations. Only the fluctuation signals require significant processing. Two schemes were used: 1) spatial filtering and 2) frequency filtering. Spatial filtering was accomplished by placing two sensors 0.3 m apart and determining the difference in their responses. method requires that matched sensors and processing electronics (both dc and ac response) be used. Frequent checks on the senors were made to insure that environmental aging did not cause their responses to differ more than is tolerable. For frequency filtering, a single sensor was used and bandpass filtering, with lower and upper cutoff frequencies of 6 and 200 Hz, was imposed. The 0.3 m seperation and the 6 to 200 Hz bandpass both insure that only fluctuation components in the inertial subrange are utilized. It is necessary to restrict measurements to the inertial subrange

since ship motions introduce signal at lower frequencies, which would lead to incorrect results if these frequencies were used for direct flux estimates.

After spatial or frequency filtering, the rms value of the fluctuation signal is obtained which is then used in subsequent calculations. It is very difficult to obtain matched sensors and to construct a difference bridge for the hot film sensors used for wind speed fluctuation measurements. Thus, only frequency filtering was used for wind speed fluctuations. Both types of filtering were used for temperature fluctuations, but the majority of the results are for the spatial filtering technique.

The third method used to process fluctuation signals was spectral analysis. This can be done only for single sensors. The power spectral density of the inertial subrange signal was determined in-situ with a real time spectrum analyzer. The results were not one of the primary analysis tools, but were used to check the validity of the results from the other techniques. For example: 60 Hz pickup would be apparent by spectral analysis, but would increase the rms signal without the operator's knowledge, and lead to erroneous results. Other equipment problems, and ship influence distortions can also be detected by spectral analysis. Thus, spectra were produced on a frequent and regular basis throughout all cruises. Spectral analysis was performed by Nicolet 440B or Federal Scientific VA500 analyzers.

Data acquisition was straightforward. Fluctuation signals were recorded on a Honeywell 5600 FM tape recorder. All mean and rms signals were acquired and recorded by a Hewlett Packard 3052A

data acquisition system controlled by an HP9825S computer. Complete cycling of the acquisition system through all signals took approximately 1.2 sec. Data was normally acquired for a 30 minute period then averaged, so that each averaging period contains approximately 1200 samples.

The computer performed in-situ calculations of meteorological parameters and recorded the data and results on magnetic tape. An immediate printout of all results was also produced. The immediate printout was very important for a successful operation as it allowed identification of portions of the system that were operating incorrectly.

III. Details of Research Cruises We report here results from five cruises:2

CEWCOM-76, 10/4-10/12, 1976; area covered was from Monterey Bay to San Diego with emphasis on the area south of Pt Conception.

ARB, 7/19-7/26, 1977; area covered was Los Angeles air basin.

CEWCOM-78, 5/14-5/23, 1978; coastal data taken but emphasis on at sea data, San Nicolas Island.

MABLES-WC, 7/31-8/17, 1978; all data taken in San Francisco area from coast to 60 N mi at sea.

Ctq, 6/2-6/8, 1979; Monterey Bay area, all data taken within 10 N mi of coast.

Charts for these cruises follow so that the results can be correlated with the ships location with respect to the coast. Dates shown on the charts indicate the location at 0000, local time, except where the time is indicated.

The chart shown for MABLES-WC covers only the time period from 8/2 to 8/4. The remainder of the time was spent along latitude 37°10'N at three stations located at longitudes: A--122°40'W, B--123°15'W, C--123°50'W. The schedule for the three stations is shown in Table 1.

Table 1. Ship schedule for MABLES-WC boundary layer study.

Date/Time	0400	1000	1600	2200
8/4			В	С
5	C	В	A	A
6	В	c	C	В
7	A	A	В	С
8	С	В	A	A
9	В	C	В	В
10	A	В	С	С
11	В	A	В	C
12	C	В	Α	A
13	В	C	С	В
14	A	A	В	С
15	C	В	A	A
16	В	С	C	В
17	A	Α		

Weather permitting, the ship sailed at full ahead between stations. It arrived at each station at least one hour before and left approximately one hour after the appointed time. The ship was positioned downwind of the station at a distance such that it would cross the station at the appointed time by sailing slow ahead into the wind. The charts for the CEWCOM-76 cruise do not show the ships location from 10/9-1100 to 10/10-1200. The only mixing rate data for which no position is shown occurred after 0700 on 10/10. During this time the ship was immediately north of Pt. Conception within 10 kmi of shore.

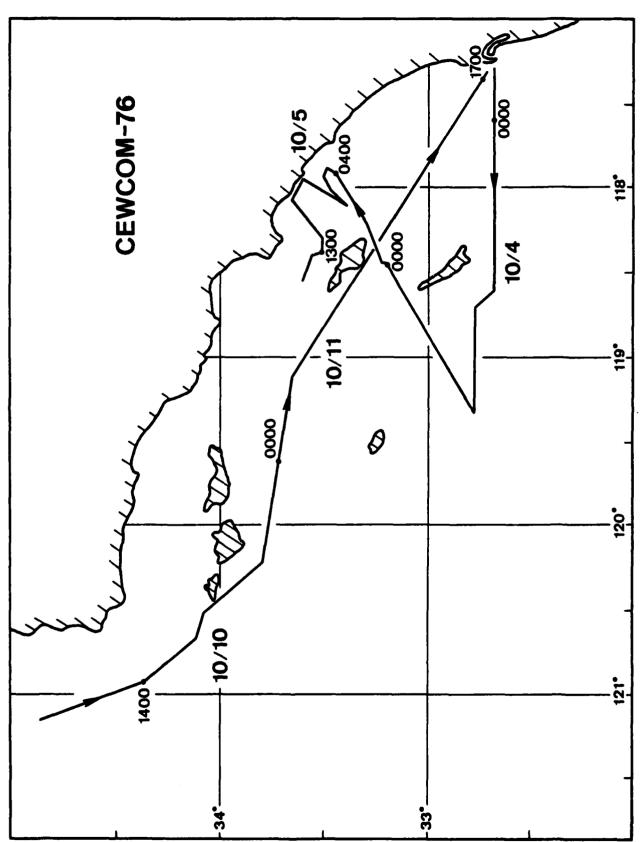
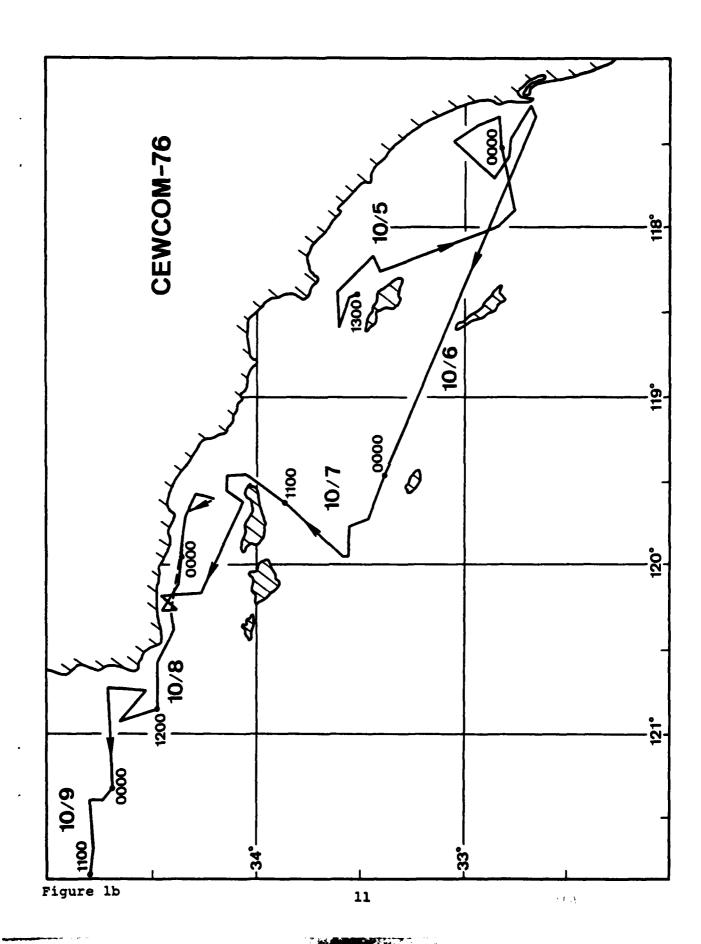
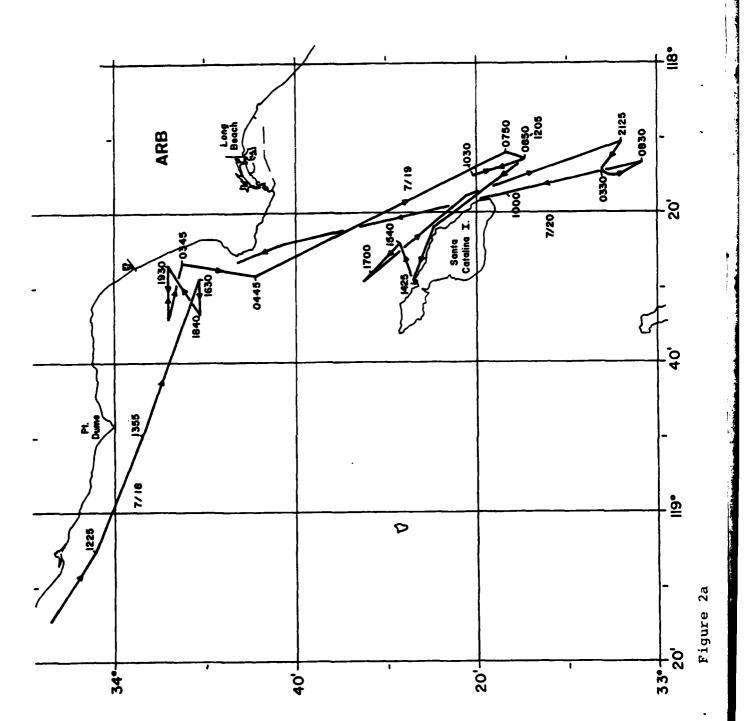
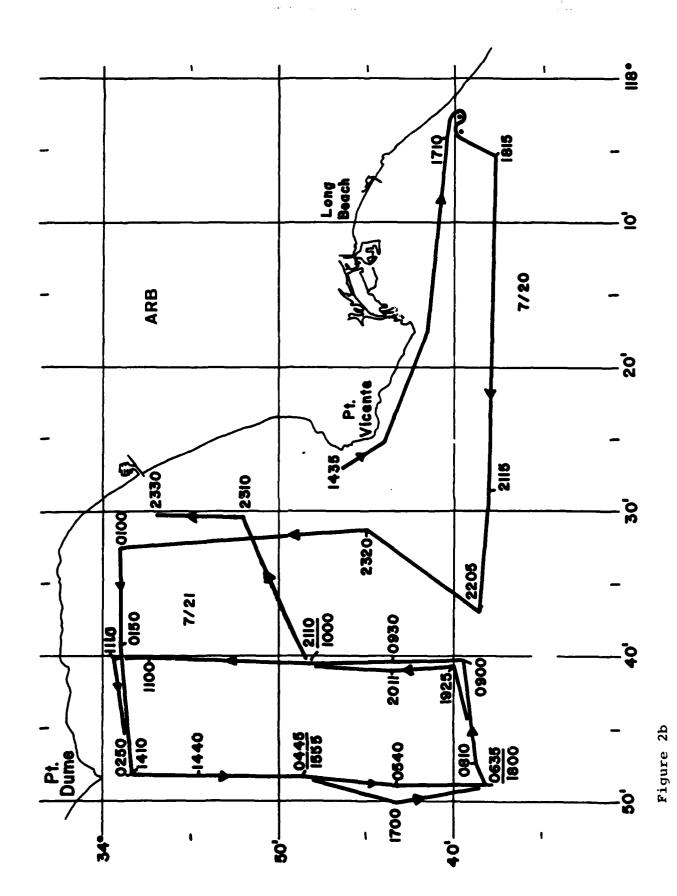


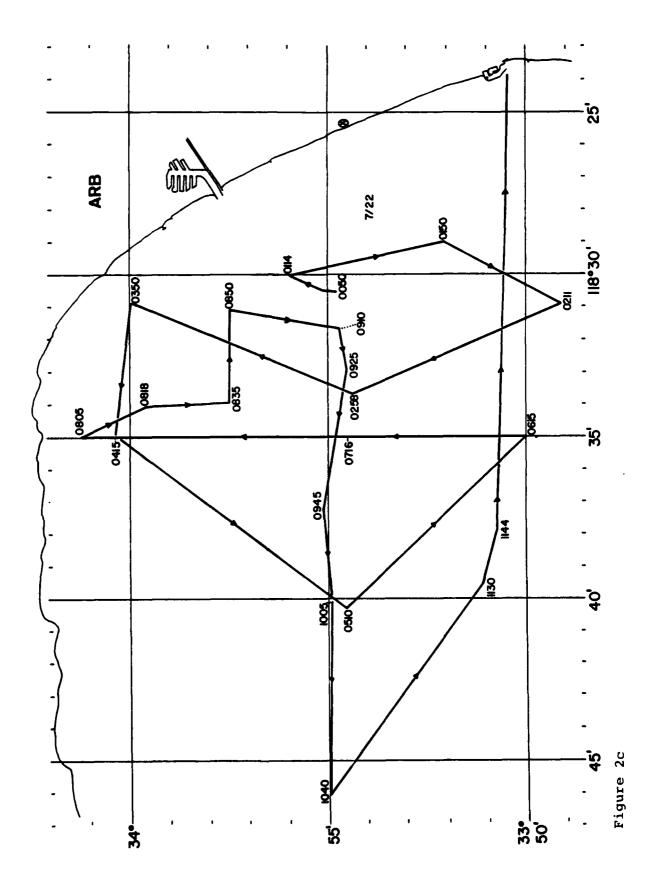
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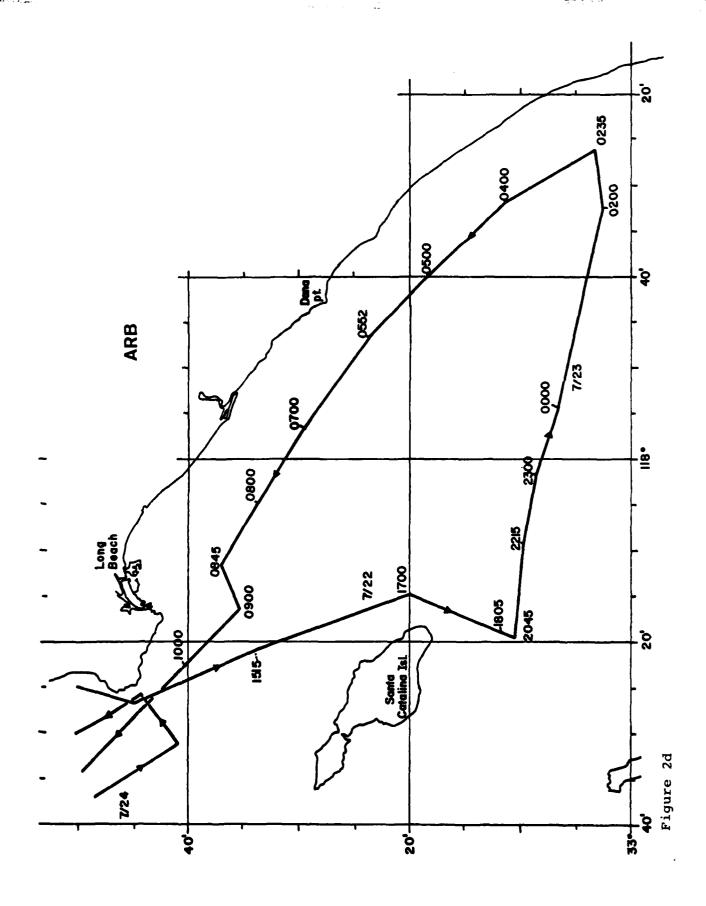






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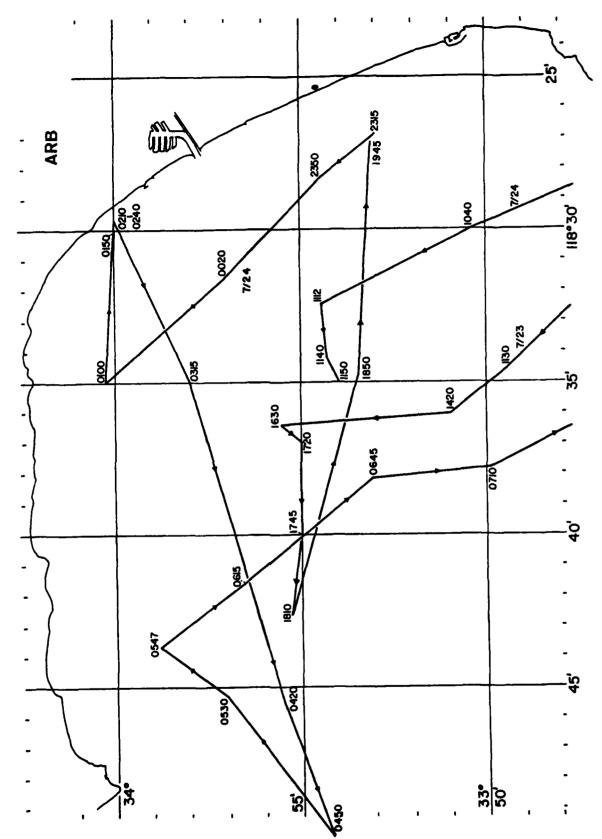


Figure 2e

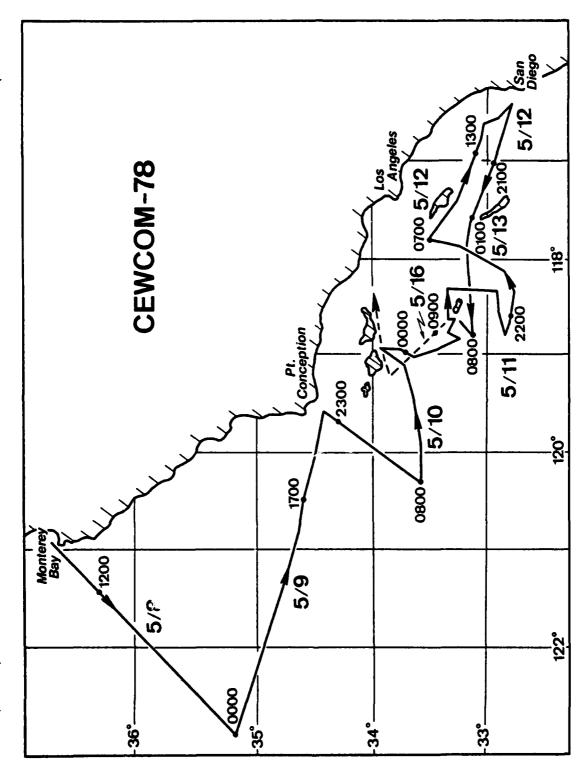


Figure 3a

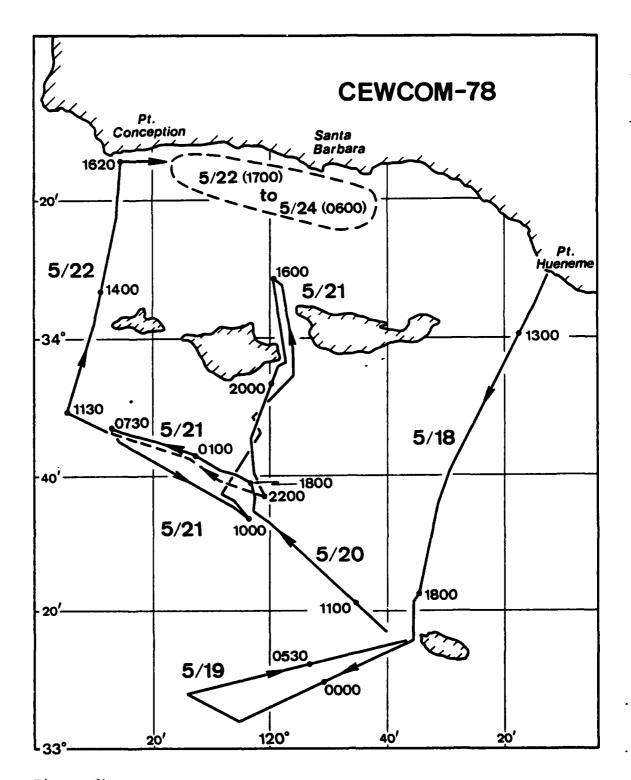


Figure 3b

MABLES-WC

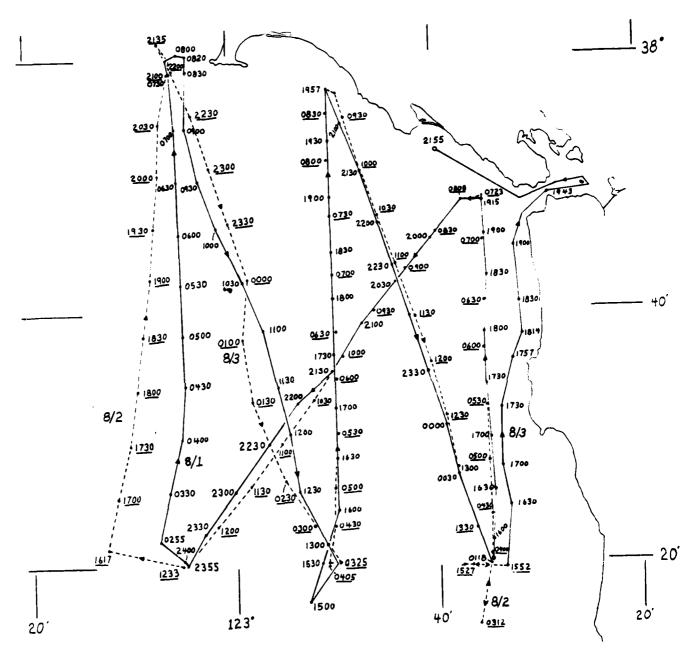


Figure 4

IV. Data Analysis

The primary purpose of this work is to determine boundary layer mixing rates and to attempt to relate the rates in a consistent manner to local conditions. For each time period, the stability, U**, T**, mixing rate, and mixing time were determined. We have found that the bulk and turbulence methods were the best to use for data analysis. Both methods were used to process these data but only the bulk results are reported. The turbulence results were used to check the validity of the output.

In this section we describe the methods used to reduce the data. The spectral analysis technique will also be described for sake of completeness. The key to the analysis is the determination of hydrostatic stability and the resultant stability correction functions that must be used to determine final parameters. As will be seen, this is an iterative process that is best done by computer.

In what follows we use the notation:

Т	temperature (K)
Z	height (m)
U	mean wind speed (m/sec)
q	water vapor mixing ratio
$\theta = T + .0098Z$	potential temperature
$\theta_{v} = \theta + .61Tq$	virtual potential temperature
g	acceleration due to gravity
κ	von Karman's constant (0.35)
k	wavenumber
f	frequency
$\alpha_{\mathbf{x}}$	turbulent diffusivity ratio ($\alpha_{u} = 1$)
U <u>*</u>	friction velocity (scaling velocity)
q*	mixing ratio scaling parameter
T _*	scaling temperature
ω _*	mixing rate
z _o	roughness length
Ł	Monin-Obukhov length
Z _i	inversion height
x	atmospheric parameter (T, q or U)
e _x	drag coefficient
ξ	Z/L
φ (ε)	gradientstability function
ψ(ξ)	profile stability function
f(ξ)	stability function

 $arphi_{\epsilon}(\xi)$ dissipation stability function $\epsilon \qquad \qquad \text{turbulent kinetic dissipation rate}$ $\mathbf{C}_{\mathbf{X}} \qquad \qquad \text{structure function}$ $\mathbf{S}_{\mathbf{X}} \qquad \qquad \text{power spectral density}$

We describe the stability with the Monin-Obukhov length

$$L = \frac{T U \star^2}{\kappa g \theta_V \star} \tag{1}$$

The scaling parameters are related to the gradients by

$$\frac{dX}{dZ} = \frac{\chi_{\star}}{\alpha_{\chi} \kappa Z} \mathcal{P}_{\chi}(\xi)$$
 (2)

Current best evidence shows that transport of the scalars, heat and water vapor, obey the same relationship to their gradients. Thus, $\mathcal{G}_T = \mathcal{G}_q$ and $\alpha_T = \alpha_q = 1.35$. The stability correction functions are:³

$$\mathcal{G}_{T}(\xi) = (1 - 9\xi)^{-\frac{1}{2}}$$

$$\xi < 0 \qquad \mathcal{G}_{U}(\xi) = (1 - 15\xi)^{-\frac{1}{4}}$$

$$= (1 + 6.4\xi) \qquad \xi > 0 \qquad = (1 + 4.7\xi)$$
(3)

Bulk Method

To obtain the stability the scaling wind speed and temperature are needed for use in Equation 1. They are obtained from bulk measurements using an integrated form of Equation 2. We integrate Equation 2 from the surface to a reference height Z, usually 10 m.

$$X_{Z} - X_{S} = \frac{X*}{\alpha \kappa} \int_{0}^{Z} \frac{\mathscr{G}_{X}(\xi)}{Z} dZ$$

$$= \frac{X*}{\alpha \kappa} \left[\ln \frac{Z}{Z_{OX}} - \psi_{X}(\xi) \right]$$
(4)

where X_{ϵ} is the surface value.

For analysis of data, it is most convenient to solve Equation 4 for X_{\star} and rewrite in terms of the drag coefficient. The neutral stability drag coefficient is given by

$$\mathcal{L}_{XN}^{\frac{1}{2}} = \frac{\alpha \kappa}{2n \ Z/Z_{OX}} \tag{5}$$

and corrected for stability by

$$\mathcal{L}_{X}^{\frac{1}{2}} = \mathcal{L}_{NX}^{\frac{1}{2}} \left[1 - \psi_{X}(\xi) C_{NX}^{\frac{1}{2}} / \alpha \kappa \right]^{-1}$$
 (6)

Thus the scaling parameter is given by

$$X_{\star} = C_{\chi}^{\frac{1}{2}}(X_{\chi} - X_{\varsigma}) \tag{7}$$

As was stated above the key to the analysis is obtaining the stability. From Equation 1 we write $\boldsymbol{\xi}$ as

$$\xi = \frac{\kappa g Z}{T} \frac{\theta \star + 0.61 Tq \star}{U_{+}^{2}}$$
 (8)

For the humidity correction term, we use $T = 15^{\circ}C$ and approximate 0.61 $T \simeq 0.18$ (q in gm/kg). Rewriting in drag coefficient form gives for neutral stability.

$$\xi_{0} = \frac{\kappa \, g \, Z}{T} \, \frac{C_{TN}^{\frac{1}{2}}}{C_{UN}} \, \frac{(T - T_{S}) + 0.18 \, (q - q_{S})}{U^{2}} \tag{9}$$

where we assume zero wind speed at the surface. Using Equations 6, 8, and 9 gives

$$\xi = \xi_0 \frac{\left[1 - \psi_n(\xi) \frac{1}{2} / \kappa\right]^2}{1 - \psi_T(\xi) \frac{1}{2} / \alpha \kappa}$$
 (10)

The procedure used to analyze bulk data is as follows:

- 1. Calculate q and q_s from the measured T_s , T and relative humidity for Z = 10 m and assuming humidity 100% at the surface.
- 2. Use C_{TN} = 1.3 x 10^{-3} and C_{UN} from the table below and the measurements to obtain ξ_0 .
 - 3. Calculate $\psi_{\rm U}$ and $\psi_{\rm T}$.
 - 4. Calculate ξ from Equation 10.
- 5. Iterate steps 3 and 4 until the desired accuracy is obtained, giving $\boldsymbol{\xi}$.
- 6. L has been determined and U_{\star} , T_{\star} , and q_{\star} are obtained directly from Equation 7.

For Z = 10 m the wind drag coefficient is found from 4

U (m/sec)	ح _{un} × 10 ³
0.3 - 2.2	1.08 U ^{-1.5}
2.2 - 5.0	0.77 + 0.0860
5 - 8	0.87 + 0.0670
8 - 25	1.2 + 0.025U

The profile stability functions are

$$\psi_{T}(\xi < 0) = 2 \ln(\frac{1+x}{2})$$
 for $x = (1 - 9\xi)^{\frac{1}{2}}$

$$\psi_{T}(\xi > 0) = -6.5\xi$$
 (11)

$$\psi_{\mathbf{u}}(\xi < 0) = 2 \ln(\frac{1+x}{2}) + \ln(\frac{1+x^2}{2}) - 2 \tan^{-1}x + \frac{\pi}{2}$$
for $x = (1 - 15\xi)^{\frac{1}{4}}$ (12)

$$\psi_{IJ}(\xi > 0) = -4.7\xi$$

Turbulence Method

The turbulence method of data analysis uses the relationship between the structure function and the scaling parameter

$$C_x^2 = X_{\star}^2 Z^{-2/3} f_x(\xi)$$
 (13)

with

$$f_{T}(\xi) = 4.9(1 - 7\xi)^{-2/3}$$
 $\xi < 0$ $f_{u}(\xi) = 4(1 + 0.5|\xi|^{2/3})$
= $4.9(1 + 2.4\xi^{2/3})$ $\xi > 0$ = $4(1 + 2.5\xi^{2/3})$ (14)

It is more usual to use ϵ rather than $C_u^{\ 2}$. They are related by

$$c_{\mu}^{2} = 2 \varepsilon^{2/3}$$
 (15)

The scaling velocity and the dissipation are related by

$$\varepsilon = (U_{\star}^{3}/\kappa Z) \mathcal{L}_{\varepsilon}(\xi) \tag{16}$$

with

$$\mathcal{G}_{\varepsilon}(\xi < 0) = (1 + 0.5|\xi|^{2/3})^{3/2}
\mathcal{G}_{\varepsilon}(\xi > 0) = (1 + 2.5\xi^{2/3})^{3/2}$$
(17)

Turbulence measurements in the inertial subrange yield C_χ^2 directly. The power spectral density, $S_\chi(k)$, of the inertial subrange portion of the turbulence is 5

$$S_{x}(k) = 0.25 C_{x}^{2} k^{-5/3}$$
 (18)

The spectral density is measured as a function of frequency. Using the frozen turbulence hypothesis $k = 2\pi f/U$ and $f S_x(f) = k S_y(k)$ gives

$$C_v^2 = 4 S_v(f) (2\pi/u)^{2/3} f^{5/3}$$
 (19)

Measuring the squared mean difference signal from two sensors separated a distance d gives the structure function directly:

$$c_x^2 = [X(r) - X(r+d)]^2/d^{2/3}$$
 (20)

If the fluctuation signal from a single sensor is bandpass filtered at lower and upper wavenumbers \mathbf{k}_{ϱ} and \mathbf{k}_{u} then the rms fluctuation signal squared is

$$(X'_{rms})^2 = \int_{k_g}^{k_u} S_{x}(k) dk$$
 (21)

Substituting Equation 18, integrating and using the frozen turbulence hypothesis gives

$$c_{\chi}^{2} = \frac{8}{3} \frac{(2^{2})^{3}}{(2^{2})^{3}} (X'_{rms})^{2} [f_{\chi}^{-2/3} - f_{u}^{-2/3}]^{-1}$$
 (22)

Thus, a measurement of the rms signal yields $C_{\rm x}^{\ 2}$ directly.

Mixing Rate

The scaling parameters described above apply to, and specify the

state of the surface layer. The surface layer momentum, heat and water vapor fluxes can be determined from scaling parameters by

$$F_{m} = U_{*}^{2}$$

$$F_{h} = U_{*} \theta_{*}$$

$$F_{0} = U_{*} q_{*}$$
(23)

The F_h in Equation 23 is the sensible heat flux. (The virtual heat flux and hence $\theta_{v_{\star}}$ is needed to calculate the mixing rate.) The depth over which the surface scaling applies is approximately |L|. Above the surface layer (ignoring the transition is the well mixed layer region), surface scaling no longer applies and new scaling length, velocity, and temperature are needed. These are: 6

$$Z_{i}$$

$$\omega_{\star} = [(g/T) Q_{o} Z_{i}]^{1/3}$$

$$H_{\star} = Q_{o}/\omega_{\star}$$
(24)

We assume that the boundary layer depth is defined by the inversion height, Z_i . Q_o is the surface virtual heat flux.

 ω_{\star} is the scaling velocity in the well mixed layer, and we assume that this velocity is directly related to the boundary layer mixing rate. Previous SF $_6$ tracer experiments performed by California Institute of Technology in cooperation with NPS have shown that ω_{\star} computed by the above method closely predicts the tracer experiment results. This is the currently available verification for using ω_{\star} as the predicted mixing rate.

The boundary layer depth, Z_1 used in Equs. 24 cannot always be taken as the inversion height. During times when there is a stratus layer, the lower edge of the stratus forms a boundary above which condensation must be taken into account in the heat balance. For such conditions Equs. 24 apply to the volume of air below the stratus, and this height should be used for Z_1 . If the inversion height is used, the calculated mixing rate will be somewhat in error. This will not be serious for most conditions since the height appears to the one third power in the expression.

RESULTS

There is no accepted, nor simple, manner to present the results of a study of this type. The parameter of interest, the mixing rate, depends on the full range of atmospheric parameters, wind, heat flux, stability, boundary layer height, etc. These parameters are influenced by proximity to land, which can also lead to diurnal variations due to the solar cycle. Since all parameters can change with time, and their variations are not simply related, one cannot relate the mixing rate to one or two basic parameters. Of course given a complete set of meteorological measurements the mixing rate can be calculated from Equation 24.

Our purpose here is twofold: 1) provide a simplified method to calculate the mixing rate from locally measured meteorological parameters, 2) catalog average values of the mixing rate that can be used to improve current air pollution models. The average values presented will be appropriate to location, time, and generalized local conditions.

Tabular data and results are presented in appendices A and B. Appendix A is the basic meteorological data: wind speed, relative humidity, air and sea temperature, and inversion height. The air sea temperature difference is included since it and the wind speed are the determining factors for the stability and heat flux. The final entry is the heat flux, which together with the inversion height, gives the mixing rate (Equation 24). Appendix

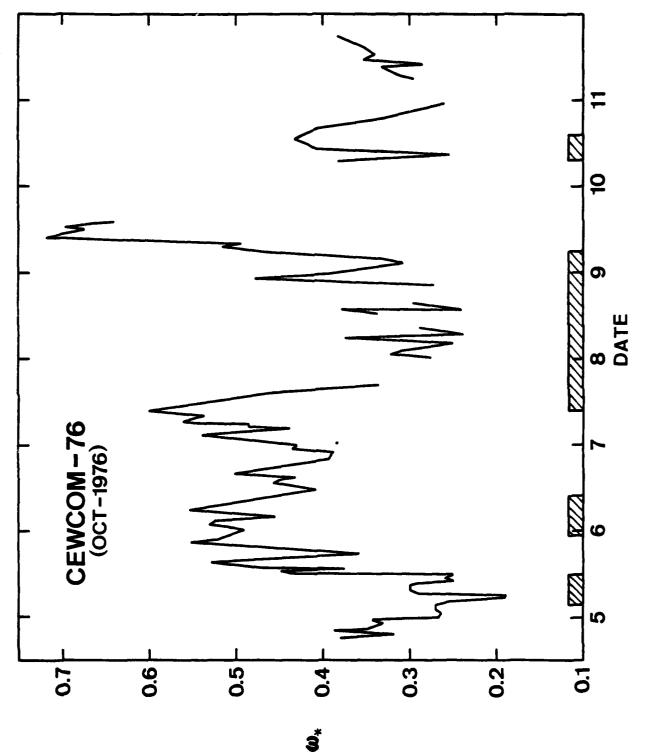
B consists mainly of calculated parameters. The wind speed and direction, and the inversion height are included as references. The wind direction is especially useful here since it can be used to differentiate local (land and sea breeze) circulations. The tables also include the stability (Z/L), the scaling parameters U_{\pm} , T_{\pm} , the mixing rate ω_{\pm} , and the total mixing time. The total mixing time is the time it takes to move a parcel of air from the surface to the top of the marine layer (or vice-versa).

Note that there are many entries missing from the tables. This is due to one sensor failing during a time period or to stable conditions. The theory is invalid for stable conditions, which occur a very small percentage of the time. The valid data for the time period is included in order to maintain as complete a record as possible.

Figures 5-9 show all of the mixing rate results, where the rate is plotted as a function of time for the full period of each cruise. All plots except MABLES-WC show these results for one-half hour averaging periods. The shaded areas at the bottom of the graphs show times when the ship was near shore. Since the Ctq and ARB cruises were mostly near shore, no shading is shown. The MABLES-WC data appears in a special format which will be discussed seperately.

Several general results are immediately apparent from a cursory examination of these plotted results:

- 1) Value range from 0.2 to 0.8 m/sec
- 2) Low values generally occur near land
- 3) Fluctuations from one one-half hour period to the next as



large as 0.2 m/sec are to be expected.

The fluctuations are attributed to both changes in wind speed and air-sea temperature difference. In many cases the ship was underway while the data was being taken, which accounts variations in observed sea surface temperature, and hence air-sea temperature difference, over short periods of time. When the ship was at a stationary location, large changes in mixing rate due to wind speed fluctuations were observed. This was especially evident near the shore.

In general, conditions along the California coast were found to be quite consistent both spatially and temporally. We now summarize the principle features of the results from each cruise in order to illustrate the important parameters.

CEWCOM-76 (Figure 5): The ship operated in the area extending from about 100 N mi north of Pt. Conception to San Diego for the period covered in this report. Near shore values of $\omega*$ were approximately 0.3 m/sec except for 10/6 when the value was \sim 0.5 m/sec due to a fairly large air-sea temperature difference ($\Delta T \sim 2^{\circ}C$). The low values on 10/5 occured when wind speed and air-sea temperature difference were simultaneously low. The rapid decrease of $\omega*$ in the afternoon of 10/7 was associated with the lowering of the inversion base as the ship neared shore (refer to Equation 24). The larger values on 10/9 were associated with a large $\Delta T \sim 3^{\circ}C$.

ARB (Figure 6): The ship operated in the Los Angeles to San Diego

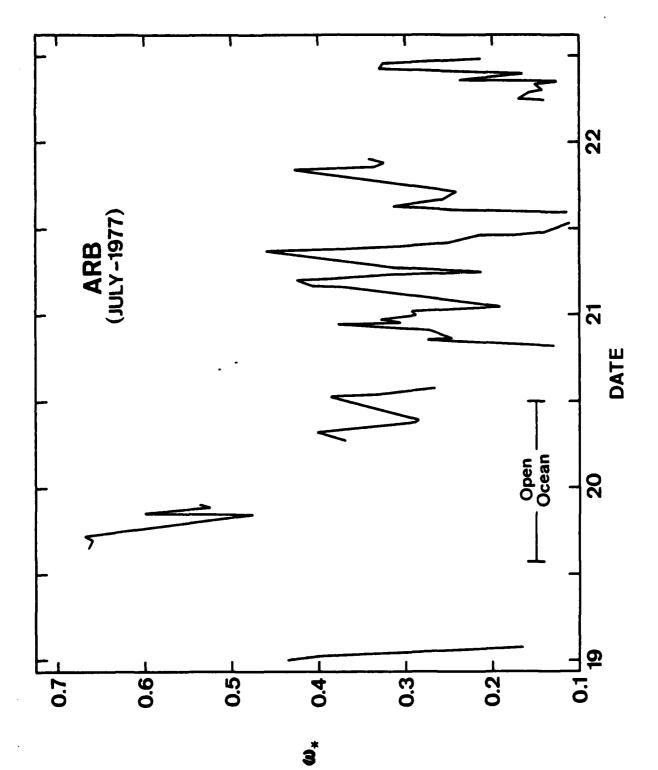


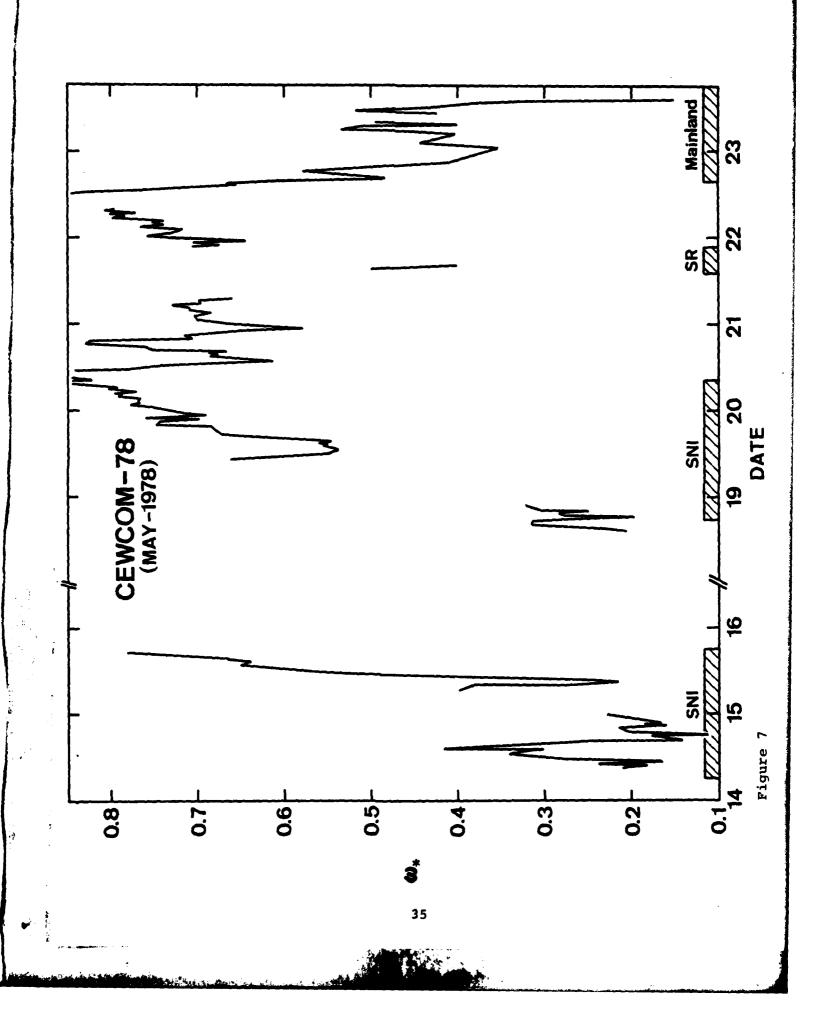
Figure 6

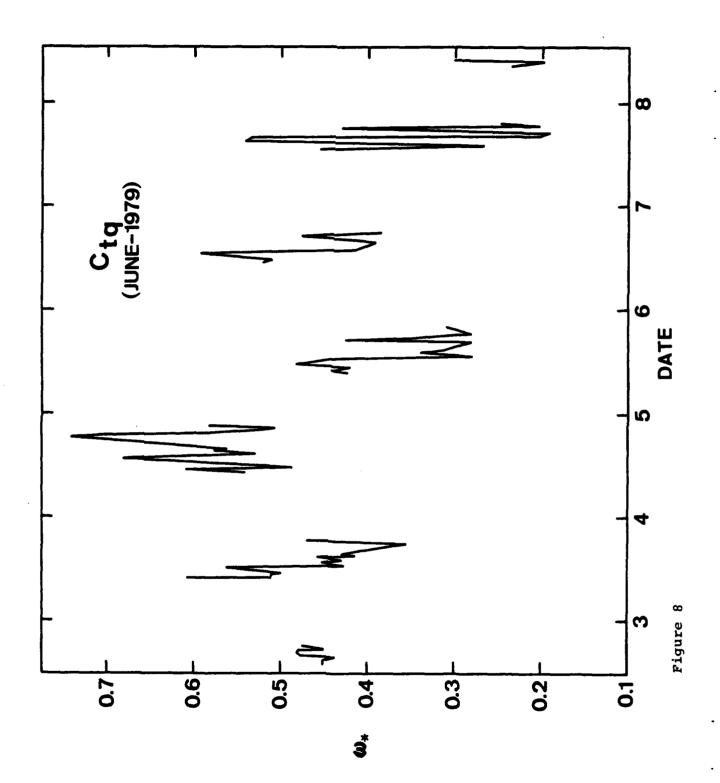
area, spending most of the time near shore. The largest $_{\omega}$ * of approximately 0.6 m/sec was observed when the ship was away from the shore on 7/19 and was associated with large ΔT values. Near shore values averaged ~ 0.3 m/sec. The very low values (< 0.2 m/sec) occured when ΔT was small, except on 7/22 when low winds resulted in low heat flux and $_{\omega}$ *. The very rapid decrease on the morning of the 19th was also associated with a decreasing wind speed in Santa Monica Bay.

CEWCOM-78 (Figure 7): This ship operated in the vicinity of San Nicolas Island, the channel islands and the Santa Barbara shoreline. Again, the lowest values for $\omega*$ were obtained when the ship was near land. Low values, ~ 0.15 m/sec, on 5/14 occured in near neutral conditions. Extremely high winds were encountered on 5/15 (up to 60 knts, when the anchor chain broke) and $\omega*$ increased rapidly. Large values, ~ 0.7 m/sec, from 5/19 to 5/22 were associated with large ΔT values. ΔT , and hence $\omega*$, decreased as the ship moved to the mainland on 5/22.

 C_{tq} (Figure 7): All data was taken near shore in Monterey Bay. The largest $\omega*\sim 0.75$ m/sec occured for a large Δ T ~ 2.5 °C and moderate winds. Lowest values and large fluctuations occured on 10/7 when conditions were near neutral.

MABLES-WC (Figure 8): The data shown is for the period when the ship was operating at stations A, B and C as described in the previous section. The data is averaged for the full time the ship





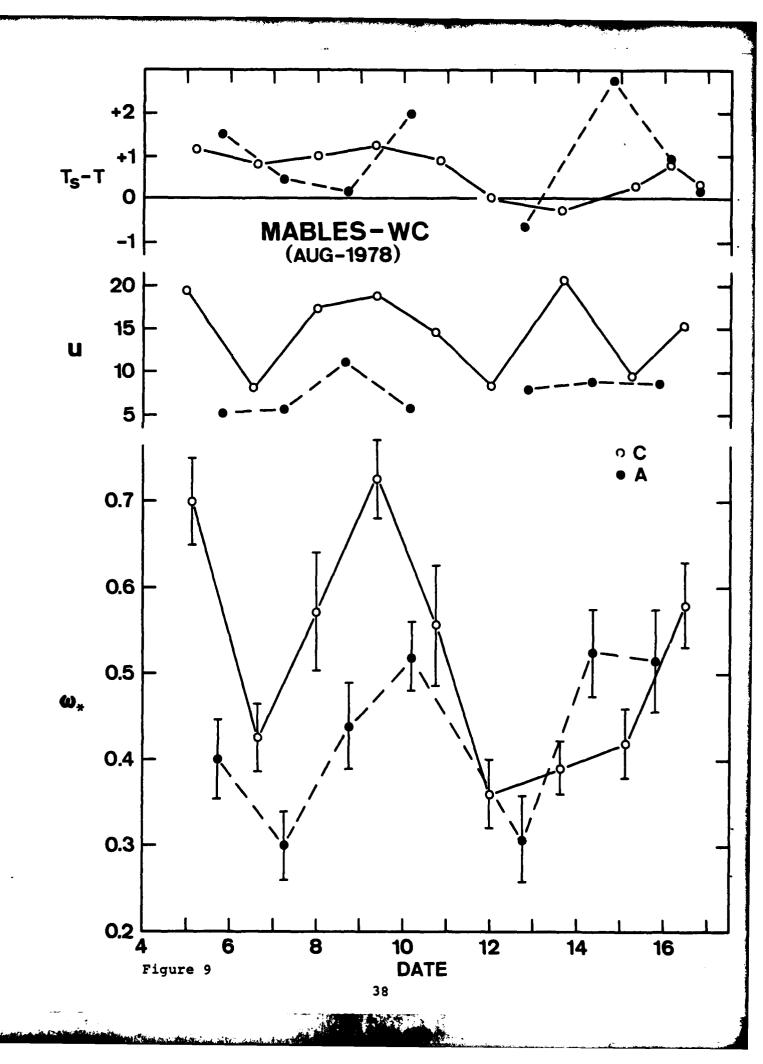
was at either station A or C, and both sets of results are plotted as functions of time. This allows an immediate comparison to be made between offshore (C) and near shore (A) locations. It is immediately apparent that offshore values of $\omega_{\#}$ are generally higher than near shore values. This is due to generally higher offshore wind speeds. The only time when $\omega_{\#}$ was higher near shore (on 8/14) was when there was a very high $\Delta T \sim 3^{\circ}C$. Along the California coast offshore winds are generally higher than winds near the shore.

We now summarize these results in a form appropriate for easy use in air pollution models. Table II presents average values of ω_* appropriate for various conditions and locations. These values can be used in place of a value calculated from measured conditions. Accuracy can not be expected to be any greater than 50% and an average avlue could be a factor of two different than the actual value.

TABLE II

Average mixing rates for various locations and conditions

Conditions	Rate (m/sec)
Open Ocean	0.7
Within 10 N mi of coast	
24 hour average	0.4
Night	0.5
Afternoon	0.6
Land-Sea breeze changeover	0.3
Strong northwesterly, any location	0.7
Low wind and air-sea temperature difference	ce 0.2



It must be reemphasized that the above recommended values for the mixing rate must be used with care. There are several commonly encountered conditions that will cause the rate to be different than that given in the table. In particular the table does not take the air-sea temperature difference, nor the magnitude of the wind, into account. We have observed ω_* to be as large as 0.9 m/sec with a large temperature difference in moderate winds. During the winter there is often little diurnal variation in the wind and a value $\omega_* \sim 0.5$ m/sec for all times is reasonable.

Of course, the most accurate means of determining the mixing rate is to use Equation 24 with measured mean meteorological data. Full utilization of this method requires the use of the correct wind dependent drag coefficient and an iterative scheme to determine the stability. A simplified calculation scheme can be used that is fairly accurate. We now outline this method and the final equation that replaces Equation 24.

Approximate drag coefficients of $\mathfrak{C}_u = \mathfrak{T}_t = 1.3 \times 10^{-3}$ can be used with the bulk method. These values are substituted into Equation 7 to give approximate scaling parameters U_* , T_* q_* . The virtual heat flux can then be obtained directly from Equation 23 and used to calculate the mixing rate. The result is

$$\omega_{\star} = 0.035 \left[z_{i} U_{10} \left[(T_{10} - T_{S}) + 0.18(q_{10} - q_{S}) \right] \right]^{/3}$$
 (25)

where $\rm U_{10}$, $\rm T_{10}$ and $\rm q_{10}$ refer to the values measured at 10 meters above sea level.

Measurements may be made at a height other than 10 meters. The drag coefficients can be easily adjusted to any reference height. Using Equation 5 we have

$$\mathbf{e}_{\mathbf{z}}^{\frac{1}{2}} = \mathbf{e}_{10}^{\frac{1}{2}} (\ln 10/\mathbf{z}_{\circ}) / (\ln \mathbf{z}/\mathbf{z}_{\circ})$$
 (26)

where Zo, the roughness length, is approximated by 6 x 10^{-4} m for wind and 2 x 10^{-5} m for temperature and water vapor. Note that corrections to Equation 25 must be applied for both the wind, and for temperature and humidity. The resulting correction for ω * is

$$\omega_{\star}(z) = \omega_{\star}(z = 10) \ 5.03[(\ln z + 7.42)(\ln z + 10.82)]^{-\frac{1}{3}} (27)$$

If a determination of sea surface temperature and inversion height is available, then the mean air parameters can be determined on shore in a region where acceleration effects are small. These measured parameters can be used in Equation 25 to give the mixing rate with an expected error of no greater than 25%. The expected error is due to ignoring the dependence of the wind drag coefficient on wind speed and the slight dependence of all drag coefficients on hydrostatic stability in the unstable regime.

Appendix A

Meteorological data: The data are arranged in chronological order for each of the five cruises. Included are wind speed, relative humidity, air temperature, sea surface temperature, air-sea temperature difference, and the calculated virtual heat flux.

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	÷	ير س	19.3	20.4	-0.43	320	5.1
	Ċ	35	19.1	19.2	-0.03	355	1.
	7	23	a.:01	19.1	-0.28	350	1.3
	5	9.0	14.5	18.0	0.53	500	-0.5
	7	16	19.1	18.6	0.50	155	-0.7
	~1	90	19.0	18.6	J. 39	120	-0.5
	5	9.0	10.0	18.7	0.23	170	-0.3
	2	37	13.0	18.7	0.25	120	7.0-
	7	96	19.0	18.7	0.23	150	-0.3
		ස හ	13.8	18.7	0, 06	140	ن.ق
	-	78	19.3	14.2	n. 05	165	0.5
	\$	63	19.3	17.7	1.57	150	٥.٠٠
	ا ئ	45	1.9.1	17.9	1.27	160	-1.1
01/26 0120) (·	18.6	13.1	0.19	90	Z*0-

~	:
1	7
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				5/1			
Jate/fine	Ξ,	199	=	<u>.</u>	υ.J 1.7 - 1.7	6.1	10+3*00
	(m/sec)	(%)	(3)	(5)	(3)	(F)	(m/sec.k)
	~	100	13.7	14.4	-1.26	3.0	-10.0
	~	100	14.4	14.4	-0.51	100	-3.1
35/14 3313	٣	160	14.3	14.3	-0.49	120	-2.3
	2	100	14.7	14.7	-0.47	140	- ا آ
	٣	96	छ • ह्।	14.6	-0.32	105	-1.7
	~	96	14.5	14.0	-0.57	35	-4.1
05/14 1051	2	96	15.0	14.4	-0, 32	06	-1.4
_	7	.j.3	11.5	15.3	-1.27	9.6	ن•ر <u>،</u> -
7	~	サケ	14.3	15.2	-1.42	άŝ	-1.4
1]	7	ታሮ	14.5	15.1	-1.06	180	-4.9
T	2	91	14.8	15.2	68.0-	280	-4.1
-	2	91	14.9	15.2	-0.78	300	-3.7
4	7	91	15.0	15.0	-0.53	310	-2.6
4	35	90	14.7	15.0	-0.82	310	-6-8
05/14 1500	4	42	14.7	14.8	-0.56	310	-3.3
বা	2	91	15.3	15.1	-0.32	310	-1.9
4	2	8.7	16.0	15.3	0.24	320	-0-3
-	m	36	16.4	15.0	₽r •0	300	1.5
	~	88	16.4	14.9	0 • 99	220	ი•0
	2	89	16.5	14.9	1,15	200	د د.
•	m	72	15.0	14.7	0.74	190	₽ • ()
	.T.	89	15.0	14.5	-0.05	160	-1.0
	*	9.0	14.9	14.6	-0.15	140	-2.1
05/14 2050	'n	3.50	14.0	14.3	0.15	125	-1 · 0
	€**	ů,ů	11.7	14.4	0.12	135	7.
	7	აე ე/	14.7	14.1	0, 05	140	- I ·
	ဝ	ა წ	14.9	14.2	.j. 14	1 40	-0.1
	ກ	187	14.9	14.1	0.24	175	-0·1
_	7	S .	14./	14.1	ú . 3)	200	-1 · 3
_		7.9	15.2	14.• 6	0° 0.3	300	7.9-
12/15 01/06	7 [19	15.4	14.6	0.13	300	-5.5
0	ತು	<i>J</i> d	15.4	14.6	0.32	300	-2.0
•	()	4 5	15.3	14.7	0.16	300	1.0
٠.	11	-	15.3	14.0	0.21	300	1.5
J5/15 9539	12	يل بن	14.0	14.6	-0.53	306	-15. v

ontr/eatr	(200/m)	<u> </u>	r' (C)	Γ3 (Ĉ)	\$1J.	Zi (m)	10+3*20 (n/seck)
05/15 1115	11	32	14, 9	14.6	-0.23	300	-5.2
05/15 1146	12	10	14.0	15.0	-0.51	300	-15.5
05/15 1216	12	د ى	14.9	15.2	-0.74	300	-18.1
j	12	35 J	15.0	15.4	-0.91	300	-20° 6
	14	 	15.0	15.5	-1.03	300	-27.1
j.	13	7.3	15.1	15.7	-1.03	300	-25.9
_	14	7.1	15.3	15.3	∯(* 0−	300	- 26 - 3
5]	14	i) ci	15.5	15.1	-(), 72	135	-25.7
	15	68	15.1	15.7	-0.72	350	-28.4
<u>5</u> .	15		15.2	15.7	-0.02	360	-32.4
ر 1	16	55	15.2	15.7	00.00	330	-36.3
ن 1	16	53	11.9	15.7	.7.1-	400	-44.3
5.1	18	99	11.5	14.9	-0.94	340	-41.0
— ≈	5	5.9	20.3	20.3	-0.53	9.0	4.0-
ຕ ຄ	٣	Ġij	20.1	20.8	-1.0v	ρç	-11.9
δ.		60	1.7.7	19,7	-0.50	99	-5.1
ත ප	ব	10 O	13.4	13.6	-0.70	09	-0.0
<u>က</u>	င	73	17.1	17.6	-1.04	6.0	-14.0
~ ~	1	70	16.7	17.2	-1.13	0.0	0.4[-
33		51	16.3	16.9	-1.1	5.0	-13.6
	(c	83	16.1	15.9	-0.27	50	-4.3
ۍ ا	£	32	15.0	16.3	-0.78	33	-7.8
~ ~	4	o r ~;	15.4	16.0	-1.01	75	
05/13 2013	m	91	15.0	15.9	-1.34	115	€ • 9 -
.ლ ე:	~	4.6	14.9	15.3	-0, 65	105	4.4
Σ	13	94	14.9	15,3	-1). 95	5.0	-19.0
ا <i>،</i> ا	ထ	æ	12.4	15.1	- 3.10	200	-42.4
05/19 1200	ī.C	94	12.1	15.2	-2.93	210	-25.3
	5	16	12.9	15,3	-2.8r	130	-25.5
ن 1	Ö	33	13.0	15.3	-2.35	170	-25.3
19	5	93	13.1	15.4	2.84	135	-25.0
19 1	9	92	13.2	15.5	-2.34	190	-25.3
]	9	92	13.3	15.5	-2.63	200	-24.5
J5/19 1500	c	55	13.3	15,5	-2.75	200	-25.8
05/10/1534	\C	50	13.2	15.5	-2.4]	160	t.07-

Date/rise	Ū	<u>-</u>	=-	:: :=	5.l. – J	2 i	10+3*10
realism specializate or the sea on the tips of the special terms to	(av/sec)	(\(\frac{1}{5} \)	(3)	(0)	(0)	(1)	(ycos/u)
35/10 1630	7	*5	13.0	15.5	-3.01	210	-32.1
05/17/20	భ	93		15.4	-3.05	220	P. CF-
05/19 1730	te	43	12,8	15.4	-3.06	240	-37.1
7	7	45	•	15.4	-3,20	250	-36.4
_	7	95	12.5	15.5	-3.43	230	6.46-
ټ	æ	96	•	15,3	-3.66	2.20	-42.0
2	က	2.7	•	15.3	-3.75	260	-47.1
(1)	·c	Lt.		15.4	-3,92	250	-50.9
05/19 2100	7	3	12.1	15.3	-3.72	240	-43.0
c	7	9.4 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0		15.4	-3.77	230	-43.2
	œ	3 .0	11,)		-3.68	230	-45.6
		55	12.0		-3.76	220	-44.0
	7	90			-3,43	210	-43.5
	7	13			-3.13	240	-44.0
05/20 0130	9	38.0	11.8	15.2	-3.94	330	-38,1
	7	٠. ج.	11.5		-4.22	310	-44.5
	c	5 5	11.7	15.3	-3.10	360	-30.9
	c	53	11.6	15.1	-3.44	340	-33.3
	.c	30	11.6	15.1	-3.05	37.0	-39.3
720	7	£:5	11.4	15.1	-1.00	360	-39.3
05/20 0430	1	15	11.7		-3.42	350	-42.0
7	£	47	11.3	15.0	-3.07	360	-37.5
05/50 0530	9	5.0	11.7	14.9	-3,63	370	-36.3
		ب د	11. 3	14.7	-3.32	420	-36.2
05/20 0n30	7	01.	11.4	14.6	-3.25	420	-34.5
	1	55	11.3	14.7		420	-37.7
u5/20 u73a	33	3.5	11.5	14.7	-3.33	400	-40.2
	~	90		1.1.7	02.8-	120	-38.4
3	-:	3.5	12.2	15.5		430	-47.9
-	•	9.5	12.4	15.5	-3.55	450	-50.0
::!	J.	01	13, 6	15.3	- 1.13	440	-44.0
755 1	70	5-X	12.0	14.1	20.5	07+	-32
/20 1	7	. :	12.7	14.6	-2.35	420	-31.0
05/20 1230	~	1.1	1,.,	11.5	-2,10	440	-27.3
`	•	;÷	12.0	1.4.1		430	-21.2

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uate/rise	(238/e)	(?)	ري) (ي)	ائج (٦)	r- rs (C)	i غ (۲)	10+3*√c (4/seck)
35/23 1100	מ	ر ب	13,3		-1.41	400	-20.1
_	÷	ა ი	15.3	14.3	-1.52	45.)	-21.0
_	9	5.	13.4	14.4	-1.53	429	-21.1
35/29 love	ග	51	13.4	14.4	-1.53	450	-21.0
	٦.	3.2	13.3	14.4	-1.53	420	-20.9
	J.	£. £	13.2	14.4	-1.70	450	-27.3
33/20 1/30	10		13.1	14.5	⊃(°-1-	9.30 *	-34.0
	7.0	ž.	13.0	14.5	50.T-	440	-32.1
•	11	<u>ن</u> 4	12.3	14.0	-2.21	420	-39.4
05/20 1900	11	ůŠ	12.6	14.5	-2.19	420	-39.2
	0.1	x 3	12.3	14.1	-1-34	3 c 0:	-23.7
	11	1.7	12.7	13.8	-1.64	360	-29.5
05/20 2100	11	g 22	12.7	13.7	-1 <u>.</u> 50	360	-26.2
	11	:0 :0 :0	12.5	13.4	-1,23	380	-22.4
05/50 2200	91	ვპ	12.5	13.2	-1.16	4 0 0	-19.9
	10	તુર	12.6	13.0	0. 91	330	-15.1
	10	87	12.5	13.0	-1.02	410	-16,3
	10	38	12.4	13.1	-1,15	330	-19.1
	10	83	12.3	13.0	-1,17	420	-20.3
	10		12.4	13.1	-1,25	200	-20.0
	יע	d 3	12.3	13.0	-1,25	520	-19.7
_	5	87	12.3	13.1	-1.23	530	-17.6
	☞	iğ.	12.3	13.0	-1.22	530	-13.0
/21	÷	v	12.3	13.0	-1,17	5 y U	-17.7
7.7	3	<u>8</u> 3	12.3	13.0	-1.13	000	-13.5
7.1	J.	6 5 5	12.4	13.0	€0•1 -	009	e.al-
_	.z.	ت د ۲	12.5	1 3.1	/ (· · l -	620	۰.51-
	Ċ	00	12.6	13.0	£ .0-	669	-15.0
7,	⇔	30	12.7	13.1	-0,35	700	-13.4
/21	1	72	12. 4	13.1	-0•34	710	-11.9
721	7	3.0	12.0	13.5	1.0.1	ċ	-14.7
7.51	7	C.	13.1	13.3	-0.87	C	-12.5
45/21 1130	1	7.1	13.1	1.5.4	-0.71	יי	-3.5
7 7	KD.	77	13.5	13.5	-10.48	ာ	<u>5•</u> 9-
05/21 1445	√C	7.5	11.3	15.4	20.1-	7 (G)	-31.7

oate/Fine	(595/c)	(S)	(C)	(C)	T-T3 (C)	i.i (E)	10+3*30 (n/sec.0)
15/21 1500	1.0	7.4	14.0	14.3	-0.84	320	-11.5
05/21 1630	æ	73	14.0	14.3	-0.70	1.40	-13.5
_	11	7.8	13.6	9.51	-2,19	430	-42.0
_	<u>د</u>	7.3	13,3	14.6	-1,31	400	-22.4
	Υ	30	13.5	14.3	-1.22	520	-I7.5
_	1.0	C.S	13,5	1 3.0	-0.35	000	-17.1
5	10	14	13.5	13.5	-0.57	609	-13.0
- = = = = = = = = = = = = = = = = = = =	11	7.:	13,3	13.5	-0.63	640	-15.1
05/22 0930	1.1	77	13.2	13.6	-0,38	600	e•61-
22	10	7.5	13.1	13.7	-1.02	530	-21,2
05/22 0160	10	7.5	13,1	13.7	-1.12	57.0	-22.1
12.2	10	7.5	12,3	13.5	-1,15	560	-20.4
22	10	76	12.7	13.2	36.0-	540	-20.2
7.7	11	76	12.6	13.2	-1.03	530	-22.0
7.7	11	7.5	12.6	13.0	Z5 •0-	59.0	-20.1
J5/22 04J0	11	76	12.6	13.0	-0.83	650	-16.1
C1	10	77	12.6	13.1	-0.80	700	-17.0
C1	1.0	7.8	12.6	13.2	-1.07	700	-19.0
~	10	78	12.6	13.2	-1, 14	700	-21.1
2.5	10	73	12.6	13.3	-1.1°	720	-19.7
7	11	7.4	12.7	13.4	-1.17	730	-25.1
	10	74	12.7	13.2	-1.05	300	-19. 0
C!	ૐ	7.4	12.7	13.1	-0.90	850	-15.d
22	10	75	12.3	13.2	-0, 51	950	-17.9
/22 0	10	73	12.7	13.1	-0.37	გიმ	-17.5
7.7.	÷	7.3	12.7	13.6	-1,40	920	-21.3
/2. 1	11	77	12.9	13.5	-1.03	080	-24.4
722 1	11	7.5	12.)	13.2	-0.85	600	-21. d
05/22 1400	10	74	12.6	12.9	-0.72	550	-16.3
/22 1	ာ	7.5	12.6	12, 9	-0-35	500	-16.4
05/22 1500		75	12.6	13.4	-1.26	350	-24.8
2	13	74	12.1	13.2	-1.02	250	-26.0
05/22 1630	12	7.1	13.1	12.0	-0.25	275	-12.2
C)	12	(J.C)	14.1	14.1	-0.54	330	-13.8
7.7	7	ر د د	14.7	14.8	-3.57	156	-12.7

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Jate/rine	ر (ع/د)	F4 (%)	ار (ت)	ုဒ (၁)	7- F3 (C)	3i (ר)	10+3*2c (a/seck)
45/23 6143	ć	6.4	12.8	14.7	-2,31	20	-26.0
	* 😎		12.4	14.5	-2.05	140	-13.1
	· p	99	12.3	14.5	-2.68	0:0	−29.8
05/23 0330	to	6.7	11.9	14.5	-3.19	ဝဌ	-44.5
	7	Ģ	12.2	14.4	40.5-	130	-10.9
	~	64	12.0	11.4	-2,85	130	-15.3
	~	65	11,3] 4 • 4	-3.57	225	
	~	Št	11.3	14.3	-2.Je	200	-19.9
~	~	5.7	12.1	14.4	-2.83	200	::•h+
	2	53	11.9	14.3	-2.98	230	-12.6
	11	51	11.9	14.3	-2.93	255	-55.4
	11	54	13.8	15.0	-1.73	5ù	-45.6
23	11	54	14.3	14.9	-1.06	140	-24.9
23	\$ T	54	14.5	14.0	-0.04	160	-15.1
53	12	6.0	14.4	14.3	-0.91	0.0	-28.5
~	11	79	14.5	14.7	~u, 65	70	-21.4
23.1	12	59	15.1	14.6	-0.02	. i.	-1.1. ∪
~	12	() ()	•	14.4	0.07	50	-9.3
05/23 1430	11	09	15.2	13.9	0.77	ာဌ	2.0
05/23 1590	12	56	•	13.8	1.72	5.U	14.3
05/23 1540	1.1	50		13.7	2.25	5.0	21.1
7	11	50	16.4	13.5	2,33	20	22.0
05/23 1620	13	64	16.4	13.3	2.59	20	23.7
35/23 1610	15	18	16.2	13.2	2.49	ÜÇ	31.5
J5/23 1700	15	5.1	10.1	13.0	2.53	Ġ.	26. u
05/23 1720	15	45	16.1	13.1	2.51	ე. ე.	30.4
05/23 1800	10	87	15.3	12.3	1.00	220	6.57
05/23 1830	17	53		12.7	1.40	200	13.7
~	13	49		12.7	1.29	180	ж Э•
_	11	20		12.7	0.07	155	-1.2
	13	53	•	12.7	-0.05	125	-15.7
23 2	12	59	12.2	12.1		100	-17.9
Û ₽7	4	90	٠	12,4	હર •ેગ- -	ઝ '	? : 9 (
/24 0	ς	52	13.9	11.7	, o • [ۍ ص	5°3
05/24 0324	~	53	13.0	31.5	1.03	9	0 • 0

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Jato/Pime	ر Sec/۱۰)	- E	· (3)	1.8 (C)	(c)	i (n)	10+3*5c (m/seck)
45/24 0404	·n	ŋ .	13.7	12.1	d. 75	3	-2.1
. #7	~	ĵ° ~	13.0	11.5	0.97	0	-0.3
J5/24 J500	15	5.0	11.0	11,2	-0.47	Ō	-27.4
24	13	7.3	10.7	10.9	73	0	-17.4
	13	76	10.8	10.8	-1.52	0	-12.1
	12	7.5	11.0	10.7	-0,18	÷	-7.5
	12	7.5	11.0	10.3	+0.23	Ċ	-12.4
	12	77	11.2	10.3	-0.12	ŋ	1.6-
	11	6.5	11.2	10.7	-0.02	၁	-6.3
	11	7.3	11.0	11.0	0.16	Ċ	-4.3
_	11	92	11.3	11,1	0. 30	ت	-2.0
	1.1	75	12.0	11.1	0.16	0	0.5
_	1.2	7.6	12.1	٥.11	0.53	C	2.5
	1.5	75	12.2	11.0	0.75	С	æ•4
	12	73	12.3	10.7	1.17	c	12.3
+7	13	73	12.4	10.7	1, 25	Э	15,3
	12	14	1.2.6	10.3	1.29	၁	14.7
7.7	13	12	12.7	11.0	1.10	;;	13.6
-	٣	81	11.3	11.0	-0.24	၁	-3.7
,	3	32	11.3	11.0	-0.15	¬	-3.1
•	e	81	11.4	11.0	-0. 06	0	-2.0
	٣	31	13.6	10.5	0.63	0	0.3
_	٣	77	12.4	10.3	1.60	0	2.9
	4	78	12.5	11.0	0.95	0	1.3
	7	80	12.6	11.3	0.40	0	1.8

101-10 POTO 8

orta/alea	n (3/860)	70	J ()	الة (5)	(A) (B)	51 (a)	10+3* jo (3/300K)
i	^ ;	100	10. F	12.7	27. T	240	7.0
01/31 1205	· ~	100	10.3	14.3	-3,50	240	13.5
	7	Ϋ́	10.5	12.1	-1.67	140	27.5
	30	9.7	10.7	11.0	-0.37	120	1.5.3
	ಌ	97	10.9	11.5	-0.59	200	23.3
	x	9.7	10.9	11.3	-0.35	230	18.0
	7	~ 5	11.1	11.9	-0.35	240	22.3
	1	15	11.1	12.8	-1.73	240	2.9.0
	ي	96	11.0	13.0	-1.9.1	220	27.5
	٥	6.7	10.3	12.5	-1.05	240	2.3.1
	' C	ر. ع	10,8	13.2	-2.47	220	20.0
	~;	£.0	1.). 5	13.1	-2.62	220	20.5
	~ ;	6 6	1.0.4	13.1	65° - 21	200	17.5
	~	96	11.2	14.3	-3,11	180	21.0
	\$	76	11.4	14.1	かび・フー	100	25.0
	ঝ	2.5	11.7	13.0	-1.25	100	1001
01/31 2034	त	33	1.1.6	12.9	-1.27	240	16.3
	-3	+	11.5	12.7	-1.12	240] +• ?
	~ 1	ŧf.	11.5	11.2	F + 10	200	~ -
	ن	ćt	11.7	11.1	e • • 0.5	300	3.1
	·2'	ů,	12.1	11.7	1 + میں	320	¥. • 4
	T) ()	12.5	12.2	11, 53	32ი	5.0
	Ç	5 m	12.1	12.5	4.27	320	-
	15) 	13.3	12.0	0.05	340	1.5
		5.7	ا: ا: •	1.2.0	-7. 10	340	· · · · · · ·
celo lo/ce		5.5	15.7	13.0	-0.25	340	13.0
	3	99	12.0	13.0	-0.37	340	15.7
	7	5.5	12.5	12.3	-0.35	360	10.0
33/01 0337	9	04,	12.4	13.0	-0.45	360	17.1
13/01 0407	, -	11	12.2	12.9	- 17	300	17.7
	Ģ	77	12.0	12.8	10.82	პიმ	7 [
	1	3.2	11.7	1.2.1	-0.46	350	17.2
13/01 0531	7	£.0	11.2	11.0	-0, 35	340	15.3
	c	÷ 6	70°	11.0	-0.71	200	ن.ر!
00/01 0637	, 	2.5	0.el	T. T.	-1.3a	220	~ = =

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seis/bies	ت	100	ij	: ::	0d +1		0.48401
	(1/390)	(;)	(0)	(c)	(;)	(r.)	(1/1031)
03/01 0/37	٣	96	16.2) u. d	J. 22	235	့ က
	·c	77	10.5	10.0	0.53	300	1.1
	चं	9.6	10.3	10.0	0,25	320	7.0
13/01 091)	~1	, , , , , , , , , , , , , , , , , , ,	10.1	11.0	40.49	340	10.0
Ξ.	7	100	10.0	11.7	-1.65	370	න ආ
	~ 3	96	10.1	11,1	-1.30	366	7.0
3s/al 1053	-	: -	10.0	11.5	-1.59	330	15.0
03/01 1123	ć.	4.7	10.2	11.0	-1.37	390	17.5
	7	:c 7	10.7	11.0	-0.43	400	12,3
02/01 1246	マ	э Э	11.4	12.3	-6.91	420	11.7
	C)	ۍ. ده	11.4	12.5	-1.02	450	10.5
	77	00	11.5	12.6	-1.05	470	12.0
	4	C 5	11.0	12.6	-1.03	430	12.9
_	m	386	11.0	12.6	46.0-	500	1 i
	~1	36	11.0	12.5	-0. 02	400	1.0.3
_	~	96	11.5	12.7	-1.13	50.1	10.5
	~1)	35	11.5	17.4	-0.73	440	1.1
05/01 1532	÷	1.3	11.4	12.0	-0.27	4 30	10.0
45/41 1559	₩.	† (-	- 1.	11.4	6.15	340	7.0
	un.	3.5	11.2	11.1	0, 14	300	7.5
	". 1"	7+	10.7	11.1	-0.44	340	13.2
	~	24	10.5	11.1	-0.62	340	7 • 4
35/31 - 1941	·~)	9.6	10.4	12.1	00.1-	350	1.1
		<u>ن</u> ر	10.4	12.0	-2,49	380	T .
		lon	10.3	12.5	-2,35	360	•
	7	100	1.0.2	12.5	-2, 25	355	
~	~	101	U. U	12.2	-7.30	330	15.5
-7	~	101	10.0	12.4	-2.37	3.50	16.0
	~	101	10,3	13.0	-2.12	400	17.5
	~,	6.7	10.0	13,3	-2.72	400	0.01
03/02 0100	~	100	10. ú	13.4	-2.13	100	4 • 17 7
	4	100	16.0	13.2	-2.5)	400	23.3
	~	100	10.5	13.0	-2.47	400	13.3
	7	101	10.4	13.1	-2.71	400	u l
00/12 030n	~	101	10.3	13.2	15.51	400	1.7.1

Jarc/File	(3) (3/26g)	(3)	(0)	(5)	(5)	zi (1)	19*3*70 (3/2634)
1211 20/27	u	leo	1.). 2	13.3	-3.10	400	23.0
	÷F	100	10.3	1 3.1	1.0.0-	770	21.3
03/62 3537	æ	94	10.5	12.3	15.3-	470	2005
	7	4.1	10.	12.3	-2.22	420	34.7
	æ	ر بن	10.4	13.1	- 2.2.3	420	2.0.5
33/62 a705	;`	22	10.5	13.2	-7.12	130	5.1.7
	n)	3.6	10.7	14.2	-3.52	435	23.5
33/02 3435	•;	<u>~</u>	1.). K	13.4	-2,61	440	7.57
	٠	6.5	1.).1	12.6	-2.20	450	11.1
35/02 0335	٠,	100	10.0	11.7	-1.72	460	6.4.7
15/32 1005	'n	36	7	11.	-1.16	470	17.0
03/02 1523	'n	, t	10.0	11.1	-1.43	470	15.0
	ŗ	97	~ ·	11.4	-1.45	470	5.5
_	~	9.5	1.1.1	12.1	99*7-	4 70	20.3
_	~	<u>ئ</u> (10.5	13.1	-2.56	170	11.5
15/12 152)	5	3.8	11.1	13.0	10.1-	470	٠. ن
_	-	3.1	71.7	12.)	-1.73	430	1.0
_	-7	33	11.3	13.1	-1.45	430	2
_	₹.	9.5	11.1	13.1	-1.65	48.0	16.0
_	٠,٥	.)]	11.6	13.0	-1.46	131	1.4.
_		32		13.1	-1.51	160	25.1
1:/12 1721	L'	93	·· [[13.2	-1.75	440	25.4
13/62 1755	٦,	<u>ب</u> 44	?:-	13.2	-1.39	440	75.1
_	. 3	7,6	10.a	12.)	•	360	30.0
_	L ⁿ	96	10.0	12.4	-2.18	100	7 7 . }
	~	2.7	0.01	12.2	-2.20	4.00	17.
	٣	47	c. c	11.)	-1.70	460	13.7
	c	2.5	٤٠.	11,3	-2.03	400	10.0
	~	3.3	¥.	1.7.	-2.33	400	1:1
		66	1.5	12.3	- 3,34	366	74.1
03/02/2155	_	9.0		12.3	- 3.45	430	11.3
	יי	9.3	C1 57	12.2	-2.05	400	12.6
C:	~	100	٠.٢	11.8	-2.43	360	12.1
04/02 2343	?	100	'Γ. Φ	11.7	-2.22	380	- · · · · · · · · · · · · · · · · · · ·
04/02 2354	m	1.)()	٠. د	11.3	-2.27	390	15.3

Jate/Pime	'ime	(מפּצ/ש)	8.1 (*)	ري (3)	ائع (ت)	ات) (ک)	2i (m)	10+3*20 (1/362K)
ì	13.61	~	50	, , , , , , , , , , , , , , , , , , ,	12.6	-2, 98	420	24.2
. ~	07 n0	بد: د	i e	· ~	12.1	-2,35		. S. L.
	12.29	· ~,	100	*** o		-2,48	440	10.0
~	300	?	100	9 . 6		-2.76	440	13.Ն
~	1326	-	100	9.)		-2.73	460	10.0
~	1402	C 1	100	10.0	•	-2.48	420	10,3
~	1429	2	100	6 6	٠	-2.74	420	16.0
/03	1459	2		•	•	-2.26	450	10.7
~	0530	2	9.8	6.7		-1.83	460	10.0
8/03	0090	2	97	æ• • •		-1,52	460	n•8
	1630	1	101	6.6		-1,19	460	5.2
8/03	1700	~	101	6.6		-1,22	450	6.4
8/03	1729	7	101			-1,13	460	ဘ. (၁
~	1758	-	101	6.6		-1.60	460	7.4
8/03	1830	c:	19	6.6	12.4	-2.55	460	11.5
8/03	030	2	95	10,5	12,3	-1.77	420	10.1
3/03	0.50	æ	86	10.6	12,1	-1.49	420	11.1
~	125	٣	60		12.4	-1.68	400	13.1
~	155	4	9.8	10.9	٠	-1.92	400	17.3
~	.230	7	66	11.0	•	-2,34	380	19.9
	300	٣	98	11.0		-1,34	340	11.5
_	330	٣	9.7	11.0	12.6	-1.59	350	10.5
	355	2	36	11.5	٠	-1.30	330	1:0, 5
~	149	~	15	11.6		-1.47	340	13.3
~	521	~	+6	11.6	٠	-0.48	350	す・フ
(i)	.632	2	95	11.6	•	-2.06	340	13.0
08/03 1	830	S	96	11.5		-1.60	280	73.0
08/03 1	900	₩.	96	13,3	•	-1.91	330	20.1
)3	2045	10	96	11.3		-3,20	240	
~	2105	7	96	11.2	•		290	14.2
33	:157	~	96	11.2	13.3		260	
03	1327	C:1	9.4	11.2	•	٠	220	10, 2
/03	:257	٦	6.7	11.3	•		250	7.8
33/93 2	2327	- 7'	3 7	11.4	12,8	_	330	14.8
/i) 3	357		55 Q.	11.2	12.8	-1,58	390	10.0

71-1117-Y

)ate/Pine	(3) (3)(1)	% (%)	-1 (C)	ري) (د)	r- rs (0)	2 j (n)	1) + 3 * 2 0 (3/8024)
33/04 0057	7	101	10.7	13.2	-2.50	160	~; ~;
	~	191	1.3, 9	13.2	-2,30	130	13.2
	~	100	10.3	13.1	-2,30	150	14.
	~	5.3	11.0	13.1	-2.16	200	17.2
		30	11.0	13.1	-2.13	2.40	13.0
33704 0327	٠,	93	10.3	13.1		200	13.0
	7	9.4	10.3	13.1	-2 - 53	240	13.6
	m	100	19.7	13.1	-2.31	200	16.5
	(7)	100	10.3	13.2		100	JA. U
03/04 0527	7	4.6	1.). 7	13.3	-2.60	200	13.7
33/34 0557	_	ф. Э	10.7	13.3	-2.57	200	16.7
	.7	9.4	10.7	13.3	-2,6]	220	12.4
04/01 0057	e:	<u>و</u> (10.6	13.3	-2.63	300	12.6
13/01 0738	C 4	G -)	1.3.7	13.2	-2,52	310	13.5
	7	98	10.4	13.2	-2.40	400	3.3
	73	įį	10.5	13.2	-2.53	140	13.3
	7	100	10.1	12.1	-2.31	100	., 1
7	2	160	ે. ત	11.7	-1.39	220	7.0
_	~	3.1	10.1	11,4	-1.30	360	12.3
_	~	300	10.1	11.7	-1,61	380	1.1
_	*	7.	10.7	12.1	-1.39	430	15,3
_	·e	93	11.1	13.0	-1,35	340	25.7
	5	7 6	7.	12.5	-1.16	350	16.2
33/34 1331	۱:2	9.7	11.7	12.4	-0.76	320	15.7
4	ν ε	· ÷	11.7	12.6	06.6-	350	5.0 10.0
	7	56	12.0	12.4		331)	20.3
	32	.c.	13.1	13.6	•	300	3.2.5
_	1.0	190	12.2	14.1	٠	320	47.0
(04]	1 ខំ	, ,	12.1	14.0	•	3.40	50°
-	<u>- 1</u>	<u>ئ</u>	12.0	14.1		320	30. غ
0.4/04 1701	?	<i>L</i> 15	12.1	13.0	-1.35	33.)	40.6
	7	16	11.3	13.º	-2.02	320	35.4
` .	Ç	9	12.1	14.0	-1.34	310	45.1
	ىد	35	12.5	13.4	-1.26	260	37.1
04/04 2018	\$	9.0	12.7	13.3	† € • U−	270	21.3

Jate/Pina	(a) (a)	(e)	7- (0)	آج (۵)	31-7 (0)	2 i (E.)	10+3*)0
35/05 0312	*	ा 0	1 3. 1	14.3	-1,16	250	W • 45
	C	7	13.0	14.3	-1.22	370	1:17
01/05 0353	•	• 0 4	13.0	14.2	-1.25	310	€ C.†
13/15 0135	Ó	C.	12.3	14.2	-1,33	255	10 · 20 · 20 · 20 · 20 · 20 · 20 · 20 ·
	ŗ	+1.		14.1	-1.33	23.0	3:1• .:
	c,	.15	12.2	14.2	-2.00	240	35.5
	10	513	11.7	14.1	-2.17	235	20°5
		1,	11.6	11.1	-2.50	310	15.5
03/05 0731	10	1.00		13.9	-2.30	330	42.7
	10	5.5	11.5	•	-2,33	340	42.3
13/05 0029	Ţ	100	11.6	14.3	-5.60	31.0	3.3.1
_	7	100	11.5	14.2	-2.63	230	0. 4. 0.
_	c i:	<u>*</u>	11.5	14.2	-2.56	300	36.45
	c	<i>\$</i> .	11.6	14.2	-2.55	310	2.4.2
_	ſ	36	11.7		-2.47	320	7.4.1
11/05 1155	Ó	47	11.9	14.2	-2,36	260	11.
_	7	47	12.0	14.2	-2.16	260	£.65
_	7	10	12.0	14.3	-2.13	250	1.98
_	\ C	c-	12.1	14.0	-1.12	250	200
_	· c	21	12.1	14.3	J 7 5 5	250	34.1
_	Ç	. 7	•	14.3	-2,21	190	31.,
_	v.z	7.0	12.0	14.0	-2.05	130	T
14/05 1510	~	2.5	11.3	13.5	5y*[-	220	11.4
_	~	2.0	1].3	13.2	-1.42	210	~ · · ·
	c.,	17	~	13.3	-1.10	230	7.
	c.	S.	11.6	13.4	-1.59	2.29	7.7
	<u>~</u>	(*)	11.5	13.3	05.1-	2.30	11.1
03/15 1923	~	100	11.1	13.3	75.6	130	***
_	~	101	11,1	13.0	्यः - -	190	
13/05 2030	~~	1:00	+1,4	13.0	-1.60	210	٠•٥
	et.	92	ر. د.	13.0	±1.41−	06-	
03/05 2127	~	ć (c	11.5	7.5	-1.26	150	· • •
03/05 2153	С.	(·	11.5		-1.1	140	•
22	_	f . c.	11.5	12.7		150	•
11/05 2259	1	7.5	. • [12.5	66.0-	155	\$ · \$

127-12-1713

Jato/Pima		 :.	٠.	<u>i</u> .	L:	, ; ;	10+3+00
	(505/2)	(,	(;)	(3)	(3)	(13)) 5005/1)
03/05 2355	.	[(12.7	13.5	C\$ *0-	269	4.4
	^	16	~ ·:	13.5	36.01	2.45	· • Þ
13/05 0035	-	01	13.0	13.4	5.0°	230	12.3
	€7	7.	13.1	14.1	5: •0-	245	13.3
	-	C.	13,3	14.0	-0.73	710	13.5
J 8/05 0203	.,•	9.0	13.2	14.2	-0.05	190	13.3
	~	., 5	13.2	14.2	20 . 1-	500	1.0.4
	~=	:	1 3. 2	14.3	el.1-	500	13.5
	~	0 11	13.3	14.3		200	10. s
	'n	2.5	13.2	14.2	-i). 17	180	11.4
	137	9	13, 2	14.3	-1.07	170	13.4
	·V	4.9	13.2	14.3	-1.13	190	14.2
	₹**	oʻr	1 4.2	14.3	-1.16	190	10.1
∂.5/00 0632	₹7	ۍ چې	13.2	14.3	-1,15	190	10.7
	-	6.5	13.2	14.3	-1.11	190	16.0
	r.	6.8	13.2	14.3	-1.05	195	19.9
	5	39	13,3	14.3	-1.02	190	17.7
	S	8 9	13,3	14.3	-0.58	190	19.6
	বা	38	13,4	14.3	-0.86	200	13.1
	8	68	13.4	14.0	-0.51	190	9. 6
03/06 0936	5	3.5	13.1	13.5	-0• 36	180	13.4
	7	3.2	13.2	13.4	-0.22	210	6.7
	~	91	13.2	13.7	-0.43	300	70 113
	C1	1,12	13,2	13.7	-0.48	300	ئ. ئ
	_	ن ئ	13.3	11.1	-0.75	300	3.7
	۲.	7.1	13.5	14.3	-4.75	310	~ .::
03/05 1305	·~	9.0	13.7	14.3	-1.11	220	् • • •
_	÷	5.5	1 5.3	11.7	-1.03	190	1.1
15/35 1429	₹*	, 4	1. 1. 1	14.0	-1.03	300	10.1
15/35 1451	~	ίď	3.	্চ • 4	= -	300	∩; ;*
13/45 1523	C1	10	c • € T	15.0	+c-l-	310	. j.
11/35 1559	~	(1)	13.,	15.0	711.	310	77.
11/05 1531	-;		13.	15.0	69.1-	300	1.7.
11/01 1653	- :-	(F)	13.9	14.)	c	3.)0	7.6
11/11 17/11	-	-	~ ~	14.	-0.33	230	7 • C

.)
3
•
-
•
-

nto/riae	(pes/c)	(%) Fe	r (;;)	ts (C)	(5)	/,i (r)	1)+34 0
30/02 3002	~	- 1-	14.1	15.1	-11. 57	230	0.0
	~		11.1	15.1	-0.57	250	± 80°
	~ `	<u>.</u>	14.3	15.0	-0.79	200	ر چ ن
14/36 2102	~	~ .	14.3	14.5	-0.23	250	7.6
	5-1	12	14.4	15.2	-0.74	098	8.1
	Ž	ا د	14.6	15.5	-0.85	260	ج * د
	7	42	14.5	٦٠.٤	-0.39	220	:3 :0
	2	42	11.6	15.4	-0,73	250	1.6
	~	71.	14.4	15.5	-1.11	240	ာ မော
	C	42	14.3	15.3	-1.02	250	7.2
	٠	⊘ :	14,4	15.4	—1 . ეი	240	÷.
	63	£6	14.5	15.4	10.01	260	10.0
	3	£	14.5	15.1	-0.01	360	11.4
		¥ S	11.5	15.3	-1.73	260	13.1
	יים	62	7.4	15.3	35.0-	230	1.1
03747 0230	c:	96	14.6	15.2	-0,53	300	
33/07 0330	2	37	14. 1	15.0	-0.54	360	6.5
	-	66	11.3	13,9	0,33	240	2,3
	, -	101	12.5	13.3	-0.74	230	2.1
	-	161	12.2	13.2	-1.33	390	3.1
	C:	101	12.0	13.4	-0.00	36 U	ਟਪ ਵਾਲ
	~	101	13.1	13.5	-1), 36	316	n.c
03/07 0759	-	23	14.∩	14.2	-0.20	290	2.1
	C :	60	14.2	13.8	o. 10	300	1:1
93/07 0954	_	١٠	11.4	14.3	90°c	355	1. 5
	~	5.1	14.3	14.3	0, 05	328	2.4
	~	74	14.2	14.3	-0.53	210	10.3
	•	44	14.2	11.7	-17. 43	250	10.3
	c:	42	14.1	15.1	-0, 32	543	5.1
15/07 1301	ż	93	1 . 1	ا ٠٠١	Lu *0-	245	7.4
	C4	92	11.2	. J. S S.	-1.33	230	ν. Α.
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$703.9133 ext{ 10} ext{ 97} ext{ 13.5} ext{ 14.7} ext{ -1.13} ext{ 340} ext{ 70.5} ext{ 10.03} ext{ 9} ext{ 99} ext{ 13.4} ext{ 14.6} ext{ -1.13} ext{ 340}$		1.0	6.7	13.7		-0,13	120	37.2
705 1003 9 93 13.4 14.5 -1.13 340	S (!)	10	16	13.5	14.7	-1,13	340	33.1
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Jate/Piae	ר	<u>.</u>		E	51 1	2.1	10+3*;
	(J) (J)	(%)	(:)	(C)	(0)	(t)	(4505/E)
	10	9.7	13.4	14.5	-1.13	330	23.2
	C	47	13.4	14.5	-1-14	330	25.3
03/05 1203	ث.	11	13,1	14.5	-1.15	340	21.0
	~;	7.6	13,4	14.5	-1.13	3:30	23.4
_	1	~	14.7	14.5	0.24	200	6.2
03/11 0530	7	£'n	11.7	٠	0, 32	240	5.2
_	ć	93	14.0	•	0.16	250	ν) •
	9	40	14.5	14.5	0.11	260	0°9
_	7	9 0 0	•	٠	0.53	230	15.7
03/11 1646	ಋ	88	15.0	14.6	1). 46	240	11.1
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٦	÷	95	11.0	•	-1). 59	230	0.64
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_	~	95	14.3	14.6	-0.22	260	13.2
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بـــ	7	96	14.7	•	0, 31	၁	5.7
_	œ	36			η, 31	200	λ.
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2	7	95	14.5	٠	-0.21	140	σ· χ
C)	2	6.7	14,3	÷.	-0.12	100	6.1
O.	4	25	14.3	4.	0.01	0	3.5
0	ش	93	14.4	14.5	-0.05	0	8.3
N	4	97	14.5	4	0.04	0	φ. 2
~	5.	96	14.6	4.	0.11	0	4.5
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2	7	96	11.6	₹.	0.17	200	6.3
~	က	97	14.2	4	-0.10	180	9.2
~	Q	26	14.1	4.	-0.21	190	χ. . ο,
03/12 0433	ι <u>ς</u> ς	30	14.1	14.4	-0.33	270	1.7
~	นา	10	14.5	14.6	-0.04	200	5.3
CI.	,~	96	14.8	4	0.20	210	3.5
~	4	2.6	14.6	4	0.09	9	3.0
	~	97	14.0	14.4	0.14	0	2.0

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Date/Fine	ס	₽		្វ.	2-73	. Z	10+3*00
	(m/sec)	(3)	(0)	(2)	(2)	(Ib)	(a/secv.)
03/12 0724		96	14.7	14.9	-0.25	120	თ•#
70 2	~	95	14. }	14.8	0,00	100	0.5
~	7	9.5	14.8	14.7	0.14	100	4.7
~	ო	40	14.9	14.1	0 . 41	၁	3.5
~1	~	96	14.3	13.9	0.35	260	4.0
	æ	9.5	14.7	13.9	0.73	၁	4.7
o.	יח	93	1.4.0	14.1	0.43	140	7.6
ر د	ব	£ (;	15.4	14.9	0, 12	0	2.2
	₹ţ	9.2	15.0	15.1	U. 4 y	Ö	2.0
04/12 1500	サ	86	15.5	15.5	-0.00	0	4.7
~ ~!	रा	+3	15,3	15.0	0.36	0	2.2
7	77	95	15,1	15,3	-0,21	140	ó . 1
7	5	3.5	15.0	14.4	65.0	0	1.2
38/12 1954	- 90	9.6	15.0	14.4	0.57	၁	1.3
1	S	(2 7	14.5	14.0	. 0.33	9	-0.4
.~	ş	9.6	14.8	14.4	0.40	240	2.2
٥!	1	315	14.9	14.1	u. 74	240	-0 - 2
35/12 2156	c	/ -	14.5	13.7	0.73	300	
-1	ೡ	16	14.5	13.5	1.05	200	-3.1
	ဆ	(, (13.3	13.7	0.17	140	5.3
	.o	٠, ن ن	13.5	14.1	-0.51	120	0.6
~1	9)7	13.0	14.1	~0.56	၁	9.4
~	æ	96	14.1	13.9	0.25	0	ڻ . و
~	7	55	14.3	14.1	0.13	ာ	14.0
03/13 0155	7	5,	14.4	14.2	0.21	0	14.0
04/13 0241	7	92	14.0	14.1	0, 55	0	11.3
03/13 0301	∵	76	14.7	14.2	0.52	Ξ	12.4
34/13 0324	æ	υ. 12	14.7	14.1	0.57	300	12.4
03/13 0353	æ	32	14.7	13.3	0.03	280	- I - V
00/13 0429	11	C! 5	14.3	14.0	0.31	200	-0. b
03/13 0456	æ	9.5	14.7	13.8	0.94	2.30	÷. [-
~	c	[c	14.3	13.7	1.14	300	Ĉ•¥-
0.5/13 0.553	œ	26] ii • · ·	13.6	1,20	330	0.41 0.41
~	æ	Τí	11.)	14.1	E : : :	310	0.0
03/13 0730	=	<u>ت</u>	15.1	14.1	× 5.*0	360	10. s

Onto/Pime	n (a/sec)	7 O	÷ ()	F3 (C)	?−°33 (3)	2i (۳)	10+5×40 (a/3@ck)
1 (7 (1) 3 3 1)		_	15.1	0-51	0.10	7	18.1
0.713 0900	: o		15.1	15.0	0.03	÷ 🙃	60.02
· ~	11	9.0	15,2	15.0	0, 22	0	٦. ٩
~	11	3.1	15.2	15.0	0.12	9	10.0
~	1.1	ij	15.2	15.1	0°0 0°0	0	10.0
~	10	3:3	15.2	15.2	0,64	0	13.1
~	11	06	15.3	15,3	a• 02	0	13.3
~	10	30 30	15.4	15.2	0.22	J	در د
~;	1.1	3.7	15.3	15.0	0. 34	9	٠.
~	_	T.	15.3	15.ປ	6,31	~	< • • • • • • • • • • • • • • • • • •
~	10	-	15.4	15.1	4, 33	240	₹ . %
~;	11	9.0	15.4	15.0	11, 35	200	77.8
~	11	20	15.4	15.1	0,37	200	۲. پ
~	16	θń	15.5	15.1	0, 35	ני	7.4
. ~ ^	10	61	15.4	15.2	U. 34	700	5.4
~	11	ر ن ن	15.5	15.2	0, 32	250	2.5
~	1.1	0.6	15.5	15.3	0.27	240	10.3
~	13)]	15.5	15,1	0.31	210	25.5
03/13 1529	1.2	9.2	15.4	15.0	0,32	200	7.5.4
,~	13	16	15.1	15.2	J. 14	200	30.0
~	13	()()	15.4	14.7	J. 7J	190	20.7
~	7,	01,	15,2	14.1	1.03	200	12.4
~	1.1		15.1	11.2	:: *	225	17.0
~ ,	12	(11.)	15.0	15.0	~ (, • n)~	360	16.2
~	_	90	14.0	14.0	€. T•2	91.5	13.1
~;	7.7	9.0	14.	13.0	ે. •	330	٥٠:١
	<u> </u>	5	1.4.	14.6	0 . 0	341)	12.6
-	<u>,,</u>	<u>.</u>	14.5	15.0	10.01	350	19.0
-24	ί.	C 30	11.4	15.5	-1:13	380	24.3
4	~	3.5	14.2	15.6	-1.4)	3.30	35.4
- -	1	T ;	13.0	15.5	-1.67	300	34.1
4	ሌ	9]	13.5	15.6	-2.01	330	23.2
₹	~	9.1	12.2	15.0	-3.75	320	19.0
03/14 0430	7	23	12.3	14.9	-2.51	320	10.1
~	?	3.3	12.1	14.9	-2.75	340	14.7

JA3663-30

Jate/rime	η (π/36¢)	(3.)	∓ (€)	rs (C)	r-1'5 (0)	2i (a)	10+3*20 (a/seck)
08/14 0534		191	11.4	11.6	10.01	240	10.6
- 1	: C1	100	11, 3	15.1	-3,33	240	15.0
- 	~		11.3	15.5	-3.67	240	15.5
-,-	C1	101	11.7	15.5	-3.31	210	15.3
ব	~1	101	11.7	15.5	-1.75	220	16.2
7	~	101	11, 3	15.5	- 3.79	240	27.4
35/14 0939	च	101	12.0	15.5	1 5.44	260	23.)
04/14 1050	ന	(۱۰	12.2	15.5	-3.31	250	17.5
<u>-</u>	C	36	12.1	15.0	- 3. 16	500	15.0
_	?	500	12.3	15.7	-3,33	220	1.1.4
33/14 1130	C1	82 F	12.5	15.8	-3.13	160	12.2
06/14 1200	2	93	12.4	16.0	10.€-	190	14.4
-T	7	67	12.4	16.0	- 3. to	190	13.7
03/14 1300	~	30	12.7	16.4	-3.72	100	14.1
ب	C1	11.	13.0	16.6	-3.50	140	1,3
05/14 1357	~1) ř.	13,3	16.3	-3.53	140	20.0
33/14 1436		0.t	14.5	17.2	-2.37	150	24.2
	'n	55	13.5	10.6	-3.13	120	33.1
03/14 1513	J.	3.5	13.1	10.0	00.2-	140	32.3
-	ಸ	17	13,3	16.1	ET. * 27	14.)	\$ 1. 5
Ŧ	\s	100	12.7	16.0	-3,25	140	11.0
	ò	+0	13.3] 6. ປ	-2.16	140	32.)
	÷	55	14.1	15.4	-1.21	110	34.1
	ţ	23	14.1	15.3	-1-22	140	35.2
	7		13, 9	14.1	-0-12	140	15.4
05/14 2000	7	£1,	14.1	14.0	0.63	100	15.2
	1	96	14.3	14.2.	u. 13	1.90	13.7
	٠,٥	92	14.5	14.5	0.03	130	13.2
	₹	۱۱	14.3	15.3	-0.51	260	13.7
	ъ.	92	14.7	15.0	-0-35	300	14.1
	'n	77	14.5	11.9	-:), 32	230	13.5
05/14 2330		12	14.6	14.0		260	5.43
∽	ᡇ	÷ 5	14.0	14.3	1) • 3 ti	250	6.1
	~	76	14.0	C. + I	-0.23	280	a.€
Jello eller	~	32	14.7	15.0	-0.33	2.90	7.5

Ca In/order	-	<u>-</u>	٠.	C) 74	0.1 +.1	.; ;	1.14.5*
	(585/1)	(*)	()	(2)	(;)	(:)	(1/:5:1)
15/10 11/50	.~1	Τ.	11.7	15.0	::	23.0	•
ា	~1	1.1	14.7	15.1	-0.47	300	: •
95/15 9330	~	÷	11.	15.2	C.C. * (1-	270	6.3
٠,	- 4	111	11.0	15.2	1.03	390	6.0
15/15 1460	: 🕶	3.0	14.5	15.1		220	-:
_	<**		14.5	15.1	\$ 1 · 0 }	150	7 • .5
.5	٠٠	0.0	14.5	15.1.	41.50	1 7:5	13.1
0.715 0530	<i>5</i>	1.5	7.4	15.1	-11.13	160	1.7
53/A3 0033	**	**	14.	15.1	10.01	2.20)
14/15 0700	~ `	65	11.1	14.)		25.0	20 20
05/15 0725	,	 ;	11.	15.1	-4.73	250	6.3
^	÷	71	7.5	14.4	-0.17	240	.73
03/15/03/30	-	0.7	1.1.1	14.7	10.01	240	
, ~	~1	~ :	1 + 1	1,,4	1: :1-	210	₹. • ~;
	78	77.7	14.5	15.5	-0 . 1	100	1.0
	C1		11.7	15.5	-0.	310	χ.•ο
11/15 1123	- :	7.1	14.5	15.1	-1.1/	330	100
	; +	. T	14.7	16.1	-1.37	53 5	٦٠ . د
13/15 1239	- -	25	11./	16.1	-1. 5.	3 50	Ť.,
	~ ^	11	14.7	15.0	E	3.50	1.4.1
		1 (14.5	15.0	= -	100	١٠٠١
	-	,2	1.4 . 3	15.5	62.1-	330	15.1
	~	ر <u>٠</u>	14.2	15.1	/ t • 1 -	زنز	15.1
	m	63	14.1	15.6	-1.57	100	· · ·
14/15 1539		<u>;</u> ;	14.2	15.3		. S.S.	
44/15 1558	સ	16	14.5	15.3	-1·01	00°5	·
14/15 1630	₹*	=	14,2	15,3	1. Se	 	12°1
13/15 1730		7,	14.1	15.3	-1.72	3.70	15.2
13/15 1321	~	-	1 4 . J	15.	-1.15	345	11.
05/15 1956	,~~	15	14.1	15.7	-1.23	310	٠, ١
03/15/1912	~	12	14.1	15.6	-1.27	355	7.0
011/15 2:103	_	1.	7.4.	15.8	30.1-	4 00	-: ·
14/15 2433	7	- - - - ·	1 4. 1	15.7	-1.57	440	17.1
35/15 2059	~	÷ \$	13.4	1.,.7	-1.51	440	I o · ·
13/15/21/31	~ 1	33	13.7	15.7	-2.01	376	5) • •3

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			1970 27 K	757.5			
Jate/Finc	7	1.1	÷	. કૃત	0,1-,1	17	10+3*,0
	(555/11)	(%)	(;)	(C)	(2)	(1)	(yese/w)
ek un	-	96	13.7	15.5	-1.13	460	5.1
	c :	36	13.6	15.5	-1.13	390	4.0
S1	2	14	13.1	15.6	-2.15	440	11.1
^	.∽	66	13.0	15.7	-3*0n	163	17.7
. 3	21	001	15.1	15.4	-2.13	440	14.0
2	S	1.6	13.4	15.4	-2.05	430	25.1
	g.	<u>ئ</u> ئ	13.4	15.2	-1.72	430	21.0
13	r3	36	13.6	15.3	-1.73	180	27.5
05/15 0250	1.3	86	13.5	15.4	`.	500	2,.4
03/10 0230	7	96	14.5	15.5	-1.12	500	26.5
.~	7	56	14.1	15.5	- I · I ·	0.3 £	6.67
. :	7	7	1.4.5	15.6		440	24.4
33/16 0352	1	. 5	14.5	15.6	-1.11	420	71.00
05/15 0130	·œ	~ .	11.6	15.6	7 - O	440	24.6
•	7	95	14.3	15.5	-11.13	450	14.3
۵	_	37	14.1	15.7	-0.)I	440	17.3
o	1	χ 33	14.1	15.5	-0.34	350	16.3
33/16 3700	1.1	45	14.5	15.5	-0.93	390	44.4
05/10 0/30	ాఫ	37	14.5	15.5	1,5.*()-	400	26.6
13/16 0754	^	7.0	14./	15.7	-1.02	330	21.5
03/15 09 ad	·o	<u>ග</u> ත	14.7	15.4	-1.7]	360	26.8
	æ	30	14.6	14.7	60°0-	360	19.3
>	5	8 8	11.3	14.7	3, 63	350	1,1
9	€.	ŝŝ.	15.0	15.2	-(1.2)	360	20.4
03/15 1053] : 1	4.0	15.0	15.1	-0.13	\$6.0	25.3
05/15 1130	•	2.5	15.0	15.1	-1). I ti	360	13.3
00/10 1/00		·ć.	15.0	15.2	-0-13	300	14.0
35/15 1233	6,	-5.5 -5.5 -5.5 -5.5 -5.5 -5.5 -5.5 -5.5	15.1	15.3	-0.16	340	14.1
03/15 1430	Lo	ويؤو	15.2	15.3	-0-13	320	15.7
03/15 1500	91	Ç, à	15.2	15.4	-6.17	330	P. C
13/15 1537	1.1	: 1	15.3	15.3	CO * 6-	240	14./
J3/16 1624	12	ζ,	15.5	15.3	-0.01	200	15.1
03/10 1024	12	36	15.3	15.3	T(*0-	200	15.1
13/10 1700	12	3.5	15.3	15.3	0.03	300	14.2
13/10 1/30	12	44	15.3	15,3	0.17	300	14.2

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Jack/files G (C) (C) (D) (A) (A/2002) Jack/files (E) (C) (C) (D) (A) (A/2002) (B) (A/2002) (B) (A/2002) (B) (B) <t< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></t<>								
1830 10 45 15.4 15.2 0.13 360 1950 11 64 15.4 15.1 0.32 360 1957 11 63 15.2 14.7 0.48 360 2035 10 63 15.3 15.3 360 360 2035 11 63 15.4 15.3 16.3 360 2035 13 15.4 15.4 16.3 360 360 2036 13 15.4 15.5 16.0 360 360 2037 14 15.5 15.5 16.0 360 360 2038 15.4 15.5 16.3 16.3 360 360 2039 13 15.5 15.3 16.3 360 360 2030 13 15.5 15.3 16.3 360 360 2030 13 15.3 16.3 16.3 360 360 <td< th=""><th>Jate/ri 🕾</th><th>ر (مولارد)</th><th>(3.) Fee</th><th>ر (5)</th><th>T's (C)</th><th>2-50 (0)</th><th>2 j (.0.)</th><th>10+3+0c (a/secs)</th></td<>	Jate/ri 🕾	ر (مولارد)	(3.) Fee	ر (5)	T's (C)	2-50 (0)	2 j (.0.)	10+3+0c (a/secs)
1900 11 64 15.4 15.1 0.32 360 1927 11 63 15.2 14.4 0.44 360 2030 11 63 15.2 14.7 0.48 360 2130 11 63 15.3 15.3 -0.39 360 2130 13 61 15.4 15.5 -0.10 2230 12 60 15.4 15.5 -0.01 2230 12 60 15.4 15.5 -0.01 2230 12 60 15.4 15.5 -0.01 2230 13 83 15.4 -0.10 2330 13 83 15.4 -0.11 2230 13 83 15.4 -0.11 2230 13 83 15.4 -0.11 2230 13 83 15.3 -0.20 2245 7 85 14.3 -0.20 2245 7 85 14.3 -0.20 2245 7 85 14.3 -0.20 2245 87 14.1 15.0 -0.20 2246 87 13.5 14.3 -0.20 2250 225 225 225 2250 225 225 2250 225 225 2250 225 225 2250 225 225 2250 225 225 2250 225 225 2250 225 225 2250 225 225 2250 225 225 2250 225 225 2250 225 225 2250 225 225 2250 225 225 2250 225 225 2250 225 225 2250 225 2250 225 225 2250 225 2250 225 2250 2250 22		2	d',	15.4	15.2	υ . 13	300	11.4
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1954 11 43 15.2 14.7 0.48 360 2036 10 63 15.3 15.3 -0.39 360 2130 11 42 15.4 15.7 -0.39 360 2130 13 61 15.4 15.5 -0.01 360 2230 12 61 15.4 -0.04 360 2230 12 61 15.5 -0.07 360 2230 12 61 15.5 -0.04 360 2230 12 61 15.4 -0.04 360 2230 13 15.3 15.4 -0.04 360 2240 13 15.4 -0.04 360 360 2250 13 15.3 15.3 15.3 15.3 360 2250 13 14.3 -0.14 360 360 360 2251 23 23 14.3 -0.23 360		7	3.2	15.3	14.4	6, 44	360	2.1
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2100 11 32 15.4 15.7 -0.39 360 2130 13 41 15.4 15.6 -0.15 360 2230 12 41 15.5 -0.07 360 2230 12 60 15.5 -0.07 360 2230 12 60 15.5 -0.07 360 2230 12 60 15.5 -0.07 360 0030 13 60 15.3 15.4 -0.07 360 0030 13 15.3 15.4 -0.04 360 0130 13 15.3 15.4 -0.04 360 0130 13 14.3 -0.24 360 0245 14 15.4 -0.24 360 0245 14.3 15.0 -0.24 360 0245 7 47 14.3 -0.24 360 0245 7 47 14.3 -0.24		7.	5,3	15.3	15.3	-0.50	360	34.
2130 13 41 15.4 15.6 -0.15 360 2230 12 41 15.5 15.5 -0.07 360 2230 12 41 15.5 15.5 -0.07 360 2230 12 63 15.3 -0.07 360 0053 11 63 15.4 -0.05 360 0053 13 63 15.4 -0.07 360 0130 13 63 15.4 -0.07 360 0130 13 64 14.3 -0.23 360 0245 13 14.3 -0.23 360 0245 1 14.3 -0.23 360 0245 7 65 14.3 -0.23 360 0245 7 65 14.3 -0.24 360 0440 6 6 14.3 -0.23 360 0440 6 6 14.3 -0.23 <td></td> <td>1</td> <td>33</td> <td>15.4</td> <td>15.7</td> <td>-0.39</td> <td>360</td> <td>36.1</td>		1	33	15.4	15.7	-0.39	360	36.1
22.56 14 79 15.5 -6.01 360 22.50 12 41 15.5 -6.01 360 22.50 12 41 15.5 -0.07 360 22.50 12 41 15.4 -0.07 360 22.50 13 15.4 -0.05 360 22.50 13 15.4 -0.05 360 22.50 13 15.4 -0.05 360 22.50 13 14.5 14.3 -0.24 360 22.50 24 14.5 15.0 -0.24 360 22.50 25 14.3 15.1 -0.24 360 22.50 25 14.2 15.1 -0.24 420 23.47 25 14.3 -0.24 410 24.51 27 14.3 14.3 -0.24 410 24.52 27 14.3 14.3 -0.22 510 24.52 24 13.5 13.5 -0.22 510 25.2 25		٠,	6.1	15.4	15.6	-()- 1::	360	36.3
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	47	91	11.5	13.9	-2.5	2.10	12.1
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	۳,	50	11.7	13.9	1.2.7-	240	3.5.
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	-+	100	11.5	13.7	-2.10	250	11.5
	is.	\$ 7	11.6	14.3	69.7-	350	18.
	un.	., <u>,</u>	11.6	13.6	-1.3)	310	14.5
	₹7"	3.6	11.4	13.5	50.2-	067	12.5
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30%	7		11.3	13.7	-1.)]	270	3.1
35/05 1057	S	95	12.0	13,5	-1.17	270	9.1
ςη/	£	95	12.0	13.4	-1.73	2.70	12,2
(1)	ż	75	1.2.0	13.3	-1.03	200	1.4.0
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	7	Ç,	7.	14.5	58.7-	250	23.0
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	ř.	7.5	2.2	13.2	2	nic T	÷.
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uate∕rime	(m/sec)	RII (8)	÷ ()	T'S (C)	1.4 1.6 (C)	2 i (n)	10+3*∪0 (m/seak)
	ית	7.5	14.0	12.9	1.07	150	0.81
35/07 1959	7	75	14.1	12.9	1.21	150	1.1-
	ی	33	13.7	13.0	0.71	150	-0.2
	C 4	9.4	11.7	13.3	-2.22	350	7.1
	7	40	13.2	13.9	-0.06	160	7.1
	æ)2	12.5	13.7	-1,22	230	11.0
	7	e]	12, 5	12.)	-0.42	200	4.
	7	93	12.7	13.0	-0.30	2.30	2.3
	~	76	15.1	14.9	0. 15	650	: :
	C1	1.5	14.5	14.9	-0.03	0.50	U• 5
	.7	76	14.5	14.0	U.23	640	U. U
		15	13.0	13.4	3.8	639	U • U
	~	ଫ୍ଟ	13.1	13.6	-6.45	036	7,7

Appendix B

Calculated results: The results are arranged in chronological order for each of the five cruises. Included are wind speed and direction, stability (\mathbb{Z}/L), the scaling parameters $\mathbb{U}_{\#}$ and $\mathbb{T}_{\#}$, inversion height, mixing rate, and mixing time. When an asterisk appears after the mixing time, it means that the relative wind was more than 30° off the bow.

t (min)	و و ه	့ လ		13						13		∞ r	- v	3 20	9	7	ص	∞ r	- ư	תר	7	6	2		11	
(Des/E)	0.283 0.383 0.317	.39	.33	. 22	. 26	.18	. 29	.30	. 29	.28	. 25	25	• L 4	0.251	.43	.45	.37	 		4	. 55	. 52	.50	.49	.50	. 53
2 i (m)	100 140 110	40	110 180	∞ ⊃) (i)	T 9	_	0	√	ا س	0	7	\mathfrak{D}	3	9	∞ .	C	~	4 -	240	\sim	C	9	\sim	\sim	Ŝ
·ρ* (κ)	-0.024 -0.052 -0.030	. 05 . 03	.03	.00	0.2	100	0.0	.03	0.05	0.04	0.04	0.00	70.0	-0.024	0.08	0.08	0.02	0.05		0.03	0.09	0.08	. o	.08	0.07	J
u* (m/sec)	0.142 0.145 0.162	. 14	.20	10	90.	80°	10	80.	200	0.5	.04	.03	70.	90.	.12	.12	.15	.16	77.	. 20	.19	, 13	.13	. 14	. 12	.12
3/2	-0.299 -0.491 -0.254	.47 .16	.15	. 22	53	. 4 d	39	.75	λ. 2 4	86.	.43	.34	. 50	. 31	96.	.90	. 25	.42	77.	.14	. 38	74	56	7	7.1	~
nd (dir)	280 310 325	\neg	O N	2 4	. 2	~ ~	2	\supset	ਰਾ ਚ	. 4	4	4	4.4	* 4	9	3	~	<u> </u>	\circ	$: \supset$	┌	2	3	\sim	~	'n
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Date/Pime		0/04-200 0/04-220	0/04-230 0/05-005	u∕35-012 0/05-012	0/05-031	ŭ/J5−032 0/05−03U	0/05-052	0/05-064	0/05-0/4	0/05-085	0/05-090	0/05-091	0/05-092	0/05-102 0/05-105	0/05-121	0/05-122	0/05-131	0/05-132	0/00-144	0/05-172 0/05-183	0/05-203	0/05-215	0/05-231	0/05-001	0/06-011	0/06-014

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t (min)	11 9 9 01	11 20 9 10	11 11 10 20 20 20	11 10 00 00 00 00 00 00 00	^ ∧ N 44.
w* (m/sec)	24.00	0.471 0.407 0.463 0.430 0.507	0.00 4 4 4 0.00 0.00 0.00 0.00 0.00 0.0	0.474 0.484 0.5864 0.562 0.536 0.526 0.455	0.276 0.322 0.248
Z i (.n)	らなてまら	700000000	900440	300 220 220 300 320 320 170 180	100 100 60
['* (K)	0.07	-0.098 -0.095 -0.022 -0.034 -0.026	020000000000000000000000000000000000000	-0.033 -0.034 -0.035 -0.040 -0.040 -0.052 -0.022 -0.052	0.00
U* (m/sec)	112	111 112 120 123 124 126	222222222222222222222222222222222222222	0.233 0.235 0.235 0.279 0.218 0.129 0.153 0.153	113
7/z	20.00 00.00 00.00	-1.495 -1.204 -0.219 -0.160 -0.099	.03 .09 .10 .08 .11	-0.106 -0.088 -0.088 -0.091 -0.240 -0.932 -0.288 -0.388 -0.346	. 23 . 44 . 17
nd (dir)	995	00000000	20001	300 300 2995 2990 330 340 360 330 360	280 310
,/ i (m/sec)	• • • •			00000000000000000000000000000000000000	
Date/Fime	0/06-024 0/05-034 0/05-044 0/06-054	0/06-064 0/06-091 0/06-115 0/06-133 0/06-143 0/06-143	0/06-201 0/06-213 0/06-223 0/06-233 0/07-003	10/07-0310 10/07-0340 10/07-0450 10/07-0530 10/07-0638 10/07-0810 10/07-1210 10/07-1410 10/07-1610 10/07-1910	0/08-001 0/08-001 0/08-011 0/08-041

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t (min)	6 11 9	ω ω ~ ~ ∞ ∞	ულ <i>ი</i> და და გა	700
w* (m/sec)	m 4 4	0.341 0.366 0.377 0.239 0.296	0.280 0.478 0.478 0.330 0.330 0.472 0.6493 0.643	69.
2 i (m)	140 160 160 120	000N4W0W40N	140 200 100 100 100 100 120 180 220 260	တေလ
T* (K)	0.06 0.03 0.03	0.059 0.029 0.029 0.029	-0.023 -0.011 -0.050 -0.050 -0.030 -0.060 -0.046 -0.093 -0.108	0.11
U* (m/sec)	.10 .08 .10 .10	11.00.00 0.00.00 0.00.00 0.00.00	0.144 0.185 0.222 0.222 0.243 0.330 0.325 0.318	26
2/L	-0.463 -0.880 -0.842 -0.254	-0.510 -0.723 -0.615 -0.379 -0.590 0.663 0.436 0.428	-0.192 -0.297 -0.297 -0.098 -0.168 -0.070 -0.035 -0.131	23 23 23
nd (dir)	711221	320 320 320 320 320 320 0	350 350 350 350 335 335 350 350 350 350	7 T T
win (m/sec)			4 4 7 7 7 7 7 9 9 7 8 8 8 8 8 7 1 1 1 1 1 1 1 1 1 1 1 1 1	
Date/Time	0/03-052 0/03-062 0/03-071 0/08-080 0/08-085	0/08-124 0/08-125 0/08-131 0/08-131 0/08-144 0/08-145 0/08-150 0/08-164		0/09-195 0/09-121 0/09-122

Date/Time	wi (m/sec)	Wind c) (dir)	7/2	U* (m/sec)	T* (K)	2 i (m)	w* (m/sec)	t (min)
709-133	6.7	340			7	260	99.	9
, D	6.7	340	-0.215	0.258	960.0-	260	0.642	7
0/10-070	4.4	330			0	360	.38	16
0/10-073	3,7	320		٦.	0	380	.34	18
0/10-082	1,0	310		0.	٥.	380	. 25	25
0/10-	3.0	320		٦.	0	340	.33	17
10-	5.0	325			0	360	.40	15
0/10-	5,1	330		7	0	340	.41	14
0/10-	0.9	350		.2	٥.	300	.43	12
10/10-1603	7.6	325		. 2		180	.40	7
0/10-	5,3	300		٦.	٠,	160	.33	ဘ
0/10-	4.9	260		7	0	80	. 25	2
0/11-0	1,5	10		0.	Э.	340	. 29	19
11-06	1.6	0		J	٥.	360	.30	20
0/11-0	1.2	0		0.	ુ.	400	.33	20
0∕11 <i>-</i> 0	1.0			•	0	340	. 28	20
0/11-1	3.4				3	260	.35	12
0/11-1	3.1			7	٠,	220	.34	11
0/11-1	4.4			0.158	٠.	160	.34	20
0/11-1	3.6		-0 . 399	٦.	٠,	200	.35	6
7	3,3		-0.459	0.116	∵	300	. 33	13
0/12-075	1.9		-1.559	0.068	-0.032	420	.37	lα
10/12-0851	2.4				•	300		

t (ain)	T # 7	<u> </u>	13	٠,	12	2 -	<u> </u>	<u> </u>	- T -	, ,	` C) '	10	10	13] :8							13			15	۲٦	15	10	φ. —	15	7.7
(3/330)	<u>م</u> س.	567.00 0.100	: -G	0.553	. 7	Ç.	٠	ე :	יי יי	• 	0.400	~	.2	٠,	~	∵1					~	~:	. 2	7.	7.	~.	٠,	٠,	<u> </u>	0.240	?	0.143
7.i (-n.)	280 339	320	470	500	490	43.0	50s	540 550	0 P C	000	230	160	130	360	350	250	20	140	160	260	741)	240	200	240	240	3.40	340	300	240	310	200	270
(X)	-0.117	-0.075 -0.0.0	-0.417		Ξ.	7	-0.023	75 0 • 0 -	760.0-	0.000	70.00 80.00 10.00	-9.053	-0.044	-1.035	-0.020	-0.013	0.036	0,041	0.042	0,013	0.007	-0.001	-0.005	-0.005	€00°.0-	-5.043	-0.023	-1). 0 30	-0,020	. U.	6 LO •0-	-0.014
*(205/E)	5. 4. 4.	0.025 0.014	.11	0.142	0.132	0.136	0.150	0. Les	0.000		77.0 77.0	0.05g	0.053	0.071	•	•	•	0.213	0.257	0.257	•	0.133	0.123	0.123	0.120	3	0.009	050.0	0.087	0.037	0.063	0.039
2/1,	-4.340 -3.200		-1.125		<u>.</u>	~	-0.210	-1.134	4.1.4	167.51	-1-0.042	-2.452	-2.502	-1.645	-1.150	-0.173	0.045	0.079	0.053	-0.004	-0.024	900.C-	-0.153	$\overline{}$	-0.140	` 🗟	-0.03]	-9, 356	-0.470	4.	TC.	-1,656
nd (air)	233	/اذ ار	214	717	215	235	217	23.1) T (26.5	250	750	145	200	220	135	275	250	270	270	27.0	230	270	250	23.0	250	302	255	254	30.5	
/i. (%/302)	1.5	•		•	•	•	•		•	•	•	• 1					•		•	•	٠	•	•	•		•	•	•	•			1.0
uate/Time	/13-000 /13-002	/13-61/	07/10-1620	1)-16	07/10-1710	-7.	19-200	_		- "	01/20-01/0			- (7	, ,				20-1	07/20 - 1540	01/20-2000	01/23-2020	1	1	7/20-	-07//	01/20-2230	1	\	7/21 - 0	/21-01	01/21-0120

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01/22-1010	2.6	260	-0.763	0.039	-0.040	240	0.330	12
01/22-1030	2.0	250	-1.309	0.071	-0.045	260	0.325	13
722-1050	0.5	305	-10.055	0.024	-0.033	260	0,213	20
07/23-1440	2.5	250	1.332	0.050	0.031	280		
01/23-1505	3.3	215	0.235	0.114	0.039	310		
07/23-1645	, c = #	512	-0.036	0.163	0.001	320	0.307	11
07/23-1725	4.9	262	-0.011	0.170	0.012	35.5	6.112	53
37/23-17:15	2.1	244	-U. 208	0.068	0.004	350	0.133	31
07/23-2340	1.7	250	1.943	0.029	0.017	500		
01/24-6040	2.1	24.1	0.527	0.052	0.017	155		
37/24-3100	1,3	27.)	0.176	0.043	0.01.7	120		
01/21-0120	1.5	2.36	10.701	0.037	0.014	170		
07/24-0240	1.7	140	0.381	0.046	ر. 1 (۱ . ن	120		
01/24-0300	1.5	136	0.455	0.041	0.015	160		
01/24-0420	١. ،	210	0.044	0.032	3.011	0 + 1		
01/54-1909	1.0	209	-0.391	0.034	0.021	165		
725-225	5.0	270	0.340	0.150	0.068	160	•	
01/25-5350	5.0	731)	0.231	0.157	0.051	100		
/26-0420	1,4	34-0	3.147	0.019	0.012	9.0		

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*	(1,000)	0.210	0.204	0.163	0.237	0.162	0.258	0.277	0.311	0.339	0.334	0.302	0.415	0.345	0.273	0.112	0.251	0.157	0.173	0.112	0.205	0.215	0.101	0.134	0, 160	0.10.0	0.035	0.223	٣.	0.337	51	₹.	C:		0.451	
:7 >		125	140	105	95	06	9.0	85	180	280	300	310	310	310	310	320	300	220	300	100	160	140	125	135	140	130	175	200	\$0.0	3:30	300	300	300	30:5	300	200
* ~	(,)	-0.622	-6,023	-0.015	1.034	-0.017	-0.064	-0.060		-0.051	-0.040	-0.026	-0.033	-0.023	-0.021	0.004	0.622	0.012	0.615	0.610	-0.004	-0.008	(E) (C)	-0.003	0.501		0.005		-). 002	100.0-	0.047	•	6,011	-6, 022	-0. nt2	500.00
#D	(2/2/2001)	0.103	0.077	٦,	$\overline{}$	0,	0.075	٦,	0.	٠.	Φ,	Ξ,	Τ.	∹	\neg		=	=	\bigcirc	=	_	$\overline{}$		0.155	£.	0.303	,	(-1	٦,	7.	-	ث	0.424	47	0.459	4.7
2/1.		-0.245	-0.457		-0.104	•	-1,586	-0.760		-1.660			•		•		0.312	0,119			-0.050	-0.075	-1.032	-0.049	-0.003	-0.001	-0.002	_) . () 1	-0.011	100.1-	0, 101	0.001	-0.119	- 1) }	0 [0] 0-
· · · · · · · · · · · · · · · · · · ·	Calle	341	171	351	351	173	351	241	241	240	242	240	61	19	240	233	239	242	239	241	241	6.0	6.1	241	241	241	242	240	235	10.7	582	244	243	237	215	G 12
7 in	(090/0)	3.0	2.3	3.0	3.1	2.0	2.1	3.0	7.5	1.9	2.2	2.3	4.5	3.3	2.1	2.5	2.5	2.1	2.4	2.3	4.6	++ ++	1.0	£.	6.9	3.2	3.1	7.5	\sim	10.5	3.5	10.4	0.11	12.0	11.7	10.3
Sace/Fise		3/11-1313	C11-11/c	((1	-1-	1-19	05/14-1121	1-1	1-12	1-13	1-13	1-14	1-1	-15	1-15	<u> 1</u>	1-1	15/11-1731	1-16	1	1	1	05/14-205)	7-1	7-1	<u></u>	1-231	45/15-1002	î	1-112	5/15-0	05/15-0335	5/15-0	13	713-100	05/15-1116
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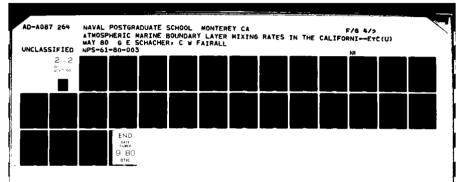
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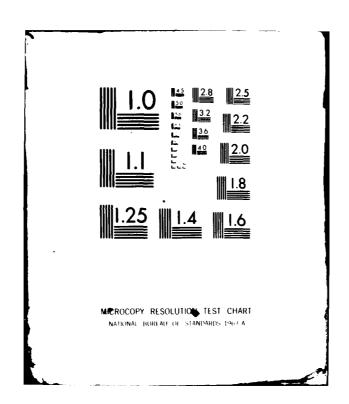
t (.i.n)	,	÷	c	11	æ	>	79	æ	ဆ	းခ	دد	'n	7	❖	ব	* ~	* ~	3 *	47	*	* '2	•	7	٣	z)	ئ.	s	Ċ	,c	୍ଦ	٠,5	ve		ত	(D
, 1/3 2C)	•	0.509		•	•		0.661		•	•	•	٠	٠	•	•	•		٠	•	•	٠	٠	•	٠	•	•	•		•	•	٠	•	0.545	•	0.612
Z.i (?1)	300	300	300	300	300	300	300	335	350	360	380	400	340	20	0.9	0.0	09	50	50	80	98	115	105	50	200	21.0	190	170	185	130	200	200	1 60	200	210
÷.	-0, 013	-0.025	-6.323	-0.622	•	-0.033		-0,022	•			-0.045	-0.931	-0.321	-0.015	-0.041	-0.035			-0.025		-0.052	-9.035	-0.032	-0.119	•	-0.111	-	-0.110	-0.109	-0.102	-0.103	-9.103	-).104	-), 194
(⊅95/8) (⊅95/8)	7.	4.	0.493	4.	٠,	ı,	i,	S.	0.612	Ġ	0.637	ŝ	. 7	ς,	~	\sim		~	\mathcal{C}	7.	_	٦.	7	٧.	٣,	7.	7	.7	0.203	. 2		~	0.224	0.239	0.272
2/1.		. 02	-0.022	<u> </u>			-0.021	1, 118	-0.016	-0.017	-0.013		-0.013	-0.770	-0.303	-0.136	-0.088	-0.109	-0.059	-0.140	-0.341	-0.654	-0.437	-0.019	. ~	-1.449	-0.403	. 32	-0.353	-0.347	13.320	-0.302	-3 -3	-0.253	-0.115
n: (-lir)	145	324	146	145	325	325	146	100	101	101	101	241	231	26	204	194	194	1.37	6.6	15	96	243	323	303	99		•		2.19	$\overline{}$		_	111	111	111
Ji (m/ses)	o:	_;	2.	Ċ	~	رب	•	4	Š	5.	ċ.	Ġ	7.						•	•		٠		•	•	•	•	•	•	•	•	•	5.9	•	•
Data/Pine	1/2	5/15-1	5/15-1	2/12-1	3/15-1	5/15-1	5-1	7	7	[-]	1-1	7	-	1	1	3-1	1	1-5	-:	3-1	7-7	3-2	3-2	3-2)-1	9-1	1-6	1-1	1	5/17-14	05/19-1430	5/19-15	5/13-15	5/13-16	05/19-1630

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,u* (a/sec)	. 64 . 67	.63 .63 .74 .75	4 2 0 2 3 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		76 76 79 78	27. 7. 0. 18. 18.	0.857 0.819 0.888 0.874 0.777 0.770 0.677 0.612
Zi (.a)	246	S C S S S	יות ותונוי	2 4 m /	() -, () () 1	とじてららるこ	460 420 420 420 440 440 415
F*	100	12 12 13 13 13 13 13 13 13 13 13 13 13 13 13			~ ~ ~ ~ .	4	-0.122 -0.117 -0.138 -0.092 -0.086 -0.072 -0.057 -0.036
(a/sec)	.30 .30	28.29	2988	23.	. 24 . 24 . 25	26 26 26 26 28	0.297 0.296 0.308 0.339 0.319 0.317 0.341
2/2	.15 .15	. 20	20 20 20 20 20 20 20	34 34 30	2 C C C C C C	26 23 30 24 24 19	-0.136 -0.180 -0.199 -0.139 -0.120 -0.069 -0.069
nd (dir)	9	ಎಲ್ಎಂಡ್ ಎ	っりょりりゃ	n ⊃ ~ − .	1 きりり:	のてらてての	270 272 1116 131 307 306 306 127
//i (a/sec)							7.6 7.6 111.5 8.6 8.9 8.9
Late/rime	5/13-1 5/13-1 5/19-1	713-13 713-13 713-20 713-20	5/19-213 5/19-213 5/19-213 5/19-223	5/13-233 5/13-233 5/20-013 5/20-020	5/20-023 5/20-030 5/20-033 5/20-033	5/20-043 5/20-050 5/20-053 5/20-060 5/20-060	05/20-0730 05/20-0800 05/20-0930 05/20-1100 05/20-1130 05/20-1230 05/20-1230 05/20-1330

t (min)	11 11 10 10				1	
w* (m/sec)	. 63 . 63 . 63	2000 2000 2000 2000	. 71 . 68 . 68 . 68 . 58	. 61 . 62 . 63 . 69	0.681 0.708 0.722 0.722 0.695 0.695	, , , , , , , , , , , , , , , , , , ,
Zi (m)	2000	1 C C 4 C C O	သာယ္ဆင္သ	18202	530 530 530 500 500 620 620	いまとするじとい
T* (K)	04	60 60 60 70 70 70 70	05 05 04 04	-0.034 -0.040 -0.041 -0.043 -0.043		200000000000000000000000000000000000000
U* (m/sec)	4446		4444	.38 .39 .39 .38	0.334 0.334 0.334 0.336 0.336	22. 22. 24. 24. 24. 25. 27.
Z/L	-0.064 -0.067 -0.065		5555	0,000	-0.053 -0.059 -0.050 -0.050 -0.058	
nd (dir)			70707	0000	301 120 301 121 301 116	インドロコンシン
win: (m/sec)		. 6 6 6 4 4 4		00446	10.2 10.2 10.2 10.0	
Date/Time	5/20-14 5/20-15 5/20-16 5/20-16	5/20-17 5/20-17 5/20-17 5/20-13 5/20-19 5/20-19	5/20-20 5/20-21 5/20-21 5/20-22 5/20-22	5/20-23 5/20-23 5/21-00 5/21-01 5/21-01		5/21-06 5/21-10 5/21-10 5/21-21 5/21-21 5/21-22





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(.n/sec)	0.643	.72	.74	.75	.73	. 92	.71	.76	.73	.75	.73	• 16	٠75	. 78	.33	. ž.	. 11	30	. 73	33.	.82	.76	.67	. 65	. 50	03.	.443	.51	<u>.</u>	• 3ó	.35	<u>, 4 4</u>	• ±3	7
Zi (m)	600 640	600	580	570	260	5 40	540	580	590	059	700	700	700	720	780	800	860	850	860	920	630	600	550	200	350	250	275	300	160	ဝၵ	50	140	000	20
T.*	-0.021 -0.022	0	•	٥.	٥.	•	0.	0.	0:	ů.	Ξ.	-0.035	j.	0.	٥.	Ξ.	0.	0.	C.	C.	-0.040	0	-0.026	Ξ.	ů.	٠.	Ξ,	С.	-:), 026		-0,035	_	-0.009	-0,113
(14/3ec)	0.377	.41	.40	.40	, 38	. 41	.39	.43	. 42	. 42	. 3ä	. 33	.40	.37	.43	.37	.34	,38	.37	.36	.43	. 44	, 39	.35	. 41	. 51	. 45	.47	. 25	.15	. 22	₹	. 23	. 31
z/L	-0.031	.03	.03	• 04	.04	.07	.04	03	.03	.03	.03	.04	.03	.04	04	.04	.04	0.4	.04	• 05	\sim	.03	. 13	•	. n 4	.02	<u> </u>	.02	10	.63		-1.020	67.	77
nd (dir)	120 302	Э	\sim 1	$^{\circ 1}$	\supset	7	3	130	0	С	\circ	\circ	3	$^{\prime}$	\supset	0	0	\circ	ټ	$\overline{}$	_	191	2	7		S	17	271	7	7	9.7	36	274	96
(n/sec)	11.7	Ή.	2	;	Ή.	<u>,</u>	2	~)	0	0	4	÷	ာ	ä	_;	.	٠. ب	•	ن	ું	ô,	7.	رب د	5	4.	ئ	1:	c:	٠	•	•	٠	•	•
Date/Fime	05/21-2300	5/22-00	5/22-00	5/22-01	5/22-01	5/22-01	5/22-32	5/22-03	5/22-03	5/22-04	5/22-04	5/22-05	3/22-05	5/22-35	5/22-05	5/22-07	5/22-37	5/22-18	5/22-98	5/22-11	5/22-13	5/22-13	5/22-14	5/22-14	5/22-15	5/22-16	5/22-15	5/22-18	5/22-20	5/23-00	5/23-010	5/23-02	5/23-030	5/23-033

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(a/soc)	0.405	0,454 0,536	0.205	0.514	0.405	0.493	0.785	0.426	0.516	0.435	0.388	0.371	0.336	0.251	0.151
2i (π)	180	130 225	200	200	200	280	255	50	140	160	60	70	90	50	20
F.* (X)	-0, 116	-0.120	-0.024	-0,126	-0,139	-0.130	-0.092	-0.049	-0.032	0,001	-0.030	-0.023	-0.002	0.005	0.027
U* (a/sec)	0.072	0.099	0.052	0,120	0,053	0.073	0.432	0.544	0.444	0.540	0.485	0.439	0.436	0.451	0.427
ч/г	-3.631	-1.971 -1.949	-1.090	-1.429	-8,048	-3.966	-0.087	-0.036	-0.043	-0.013	-0.032	-0.033	-0.017	-0.015	0.001
Jind c) (Jir)	302	307 302	299	290	291	271	269	96	275	277	274	96	95	9.8	274
Ji (<i>n/sec</i>)	4.1	4.4 0.8	1.5	3.1	1,3	2.1	11.1	13.1	11.3	14.6	12.9	12.1	14.3	13.5	11.7
Jate/fiss	05/23-0500	05/23-0544 05/23-0543	05/23-3627	05/23-0645	05/23-0700	05/23-0725	05/23-0810	05/23-1048	05/23-1130	05/23-1200	05/23-1230	05/23-1300	05/23-1333	05/23-1400	05/23-1430

t (aia)	1.1	·u	o ·			7	၁	9 '	~	•	*	* '	* •	·S	~; "	~3	\$	13	lο	† †	T3 *	* 7T			n I				* 0.1	¥ 0.1	* 0T	¥ 01	* _	, הב
(a/sea)	0.400 0.542	ر. در	. 42	ري. دي.	. 52	0.550	· o l	0.590	0.574	. 5.7	. 53	∵	. 50	. 51	. 333	. 51	0.487	. 33	. 31	. 37	.40	. 45	् य	• 52	ú. 545	.53	٠ ي	. 59	0.601	7	. 53		~	6/1.0
::i	250 240	140	170	200	230	240	240	220	240	220	220	200	180	160	100	240	240	260	300	320	320	320	340	340	340	340	350	300	360	3აი	350	340	200	220
* (/)	-0.373	-0.05v	-0, 007	-0.013	-0.005	-0.025		-0.067		-0.03	101.	-0.105	-0.125		-0.042		-0.034	•	•	•		0,015		0.002	-0.005	-0.003	-0.007	•	. OI	٠	-0.011	-0.007	-0.020	-0.049
(205/e)	0.050 0.104	0,234	0.295	•	•	•	0.232			•		0.098	•	•	0.147	0.143					•	0.177	•	•	0.201		•			•	0.241	•	•	•
3/6	-4.436			~	-0.105	_	C.	-0.399	4	_	1.0	**	<₹		S	' 2		. 7	5	হা	٣.	~	-0.275	~!	\sim	-0.211	-0.186	-0.267	-0.250	-:0.246	7.	-0.161	-0,235	-0.567
nd (lir)	293	294	300	305	313	292	287	270	274	267	25 ₈	245	232	240	20:4	275	263	270	270	277	239	301	307	2.9.3	300	307	301	30.5	302	303	308	311	314	356
/ind (a/sec)	1.5 3.0								٠			•						•					•	•	•	•	•	•	•	٠	•	•	6.1	•
orto/Fino	07/31-1135 07/31-1235	7/31-122	7/31-132	7/31-135	7/31-142	7/31-152	7/31-155	1/31-162	1/31-155	7/31-112	1/31-175	1/31-132	061-18/1	7/31-193	1/31-200	1/31-203	7/31-219	//31-213	1/31-220	1/31-223	1/31-230	1/31-233	3/01-105	3/31-312	ز10-16/ئ	3/01-022	3/01-025	4/01-033	3/11-040	3/31-043	4/31-350	5/01-10/s	ل قرا –	5/31-003

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u* (0/390)	0.431	35	.33	. 43	.47	• 44	• 58	. 61	. 55	. 55	. 54	. 59	. 59	. 54	. 54	. 56	. 52	. 53	.43	. 42	• 49	. 44	.49	. 48	.49	. 53	. 58	. 59	. 62	.63	. 65	• 68	. 62	. 60
Zi (m)	240		\sim	47		9	œ	G		N	S		\mathbf{c}		9	0	~	3	₹	\circ	4	47	9	∞	9	S	∞	S	0	0	0	0	0	0
(>) (>)		02	. 01	. 02	. 06	• 05	.05	. 04	2	. 02	. 03	-0.035	. 03	.03	.03	4	. 02	00.	. 01	0	. 01	. 01	• 06	. 11	. 10	.03	9	.09	. 11	. 10	. 10	-0.099	• 09	-
U* (m/sec)	0.095	. 17	.13	.11	. სა	.05	.13	.16	.13	. 12	.10	. 12	. 12	. 11	.10	.09	.10	• 16	. 14	. 15	.14	.09	.07	.04	.05	.07	.09	• 09	.09	.10	11	13	• 10	.08
2/5	-1.437	14	.30	S	99	. 63	.89	.51	~	32	ಌ	. 33	ŝ	. 98	18	.67	.00	, 35	.32	.26	.44	.29	3.50	. 24	8.15	3.80	2.19	.19	.53	.10	8.	4	1,85	.23
nd (Jir)	31	~ —	103	83	S	1	\sim	3	0	0	_	_	9	\mathbf{a}	203	\sim	3	4	2	\sim	4	\sim	\sim	8	\sim	2	\sim	~	$\overline{}$	7	8	g	6	S)
انبه (m/sec)	2.8 2.8			•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	٠	•	•	•	•	•	•
aste∕rime	33/01-0707	3/01-081	3/01-034	3/01-091	3/01-034	3/01-102	3/01-105	3/01-112	3/01-115	8/01-124	3/01-131	3/31-135	3/31-142	3/31-145	3/01-150	3/31-154	3/01-169	3/01-163	3/31-165	3/01-173	4/31-182	3/01-190	3/01-194	4/31-204	3/01-213	3/01-220	3/01-224	3/01-231	4/01-234	8/02-003	8/02-010	8/02-013	/02050	8/02-023

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03/02-0336 2.9 195 -2.463 0.099 -0.118 400 0.638 10 08/02-0434 4.1 187 -0.893 0.115 -0.115 400 0.673 11 08/02-0434 4.1 184 -0.784 0.151 -0.105 410 0.673 10 08/02-0537 6.7 181 -0.784 0.196 -0.105 420 0.673 10 08/02-0537 6.7 181 -0.784 0.181 -0.084 420 0.750 9 08/02-0537 5.7 187 -0.181 -0.081 420 0.750 9 08/02-0536 3.5 184 -0.185 -0.141 420 0.750 9 08/02-0536 3.5 1.98 -1.423 0.181 -0.141 420 0.750 9 08/02-0415 3.5 4.8 2.0 0.181 -0.141 420 0.750 9 08/02-0416 0.0 0.181	Date/Time	Wil	nd (dir)	7/z	(m/sec)	T* (K)	2 i (m)	w* (m/sec)	t (min)
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nd (dir)		256	270	264	254	569	253	251	258	260	200	247	265	230	227	256	221	134	175	234	162	157	284	300	307	308	301	320	328	315	315	321	330	324	323	327
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Date/Pime		C1-CC/	2	3	33/35-1725	73												7-005	1-111	7-113	1-115	1-323	1-133	7-032	7-050	7-051	7-055	17-162	7-075	3/37-355	737-035	3/07-1	7-112	

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u* t 1/sec) (min)	0.423 10 0.395 10	120	j. 652 5	J. 612	1.557	. 520	0.575	j. 563	. 10	0.021	1.659	0.030	3.650	1.640	J. 620	1. 639	0.651	0.0.1	•	-	٠		٠	•• •••		9.339	0.633	0.042	0.533 0	٠٤,	3	0.534	-1
Zi (m)	245 245																															220	550
F* (A)	-0.032	-0.053	\sim	-0.075	-n. 073	-0, 050	-1.05/	-0.054	-0.0-	-0.053	-1) • Gold	-0.054	-0.070	-d, u66	-0.043	1.0.052	-0,050	-1, (i)	-0.623	-11.011	- 1. ()] 3	-0, 0% j	-7,012	0.015	0.00	-0.030	1.0.0-	-0,012	-0.035	-:). 0.34	-9, 030		
u* (a/sec)	0.078	0.000	0.237	1.195	0.154	0.117	0.132	0.191	0.413	0,213	0.244	0.230	0,223	0.198	0.210	0,236	0.242	0.235	0.253	0.242	0.234	0.235	0.270	1.252	0.421	~	(:, 4].4	0.337	0,333	0.347	0.364	\sim	:
2/L	-2.527	~	-4.332	-0.527	-0.124	.05.0-	-1.167	1.84.0-	-0.395	-0.4.00	-0.209	-4.331	-0,332	69+*0-	-0,342	-0.234	-0.237	-0.303	-1,111	-0. loa	7.50.0	-3.47.1	-0.030	-0.103	650.01	-0.0.5	-).152	-0.071	790.0-	-0.030	F. O. D.	-0,150	•
nd (āir)	338	311	233	30.3	293	253	316	310	3:17	31.0	717	97.4	302	3.1,1	315	3.1.5	324	315	: 13	11.2	315	31.	311	320	310	300	31.1	313	315	303	310	310	
di. (عاد/))	2.5		? . ?	3.5	٠	1.3	5.5	ر. در	() ()	J. J.	~ · · · · · · · · · · · · · · · · · · ·		5.5	5.0	D. C	0.0	D . D	0, 0	7.1	G. 6	0.0		1.1	7.1	11.1	10.4	10.3	10.2	10.0	ر ق	0.0	9.0	
Date/rine	03/07-1241	7	Ī	-	1	15/1/-1501	11/11-11/16	10/1-/1/16	31/11-1131	11.1-11/15		1-/(11/11-11/10	01/37-133.	15/01-1355	13/41-2050	15/11-2.155	-/ !!		-//	-1	ı	03/31-2323	38/11-2356	Ξ	03/13-1221	36/13-0253	0.3/0.3-131	38/98-9430	03/14-0130	04/03-045)	06/06-1533	•

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(200/b)	0.535 0.628 0.733				9	9	3.0	9	• · •	ů.	• u	, বা	. 4	4	4.		~	٠,	, 4,4	٠,	٠,	٠,		٣.	7
2 i (n)	260 230 320	00	22	4 4	2 ~	∞	40	4.	40	\circ	0	0	0	\neg	-	40	S	5	\sim	J.	4	က	-	Û	
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1)* (.a/sec)	0.347 0.369 0.362	.33	36	37.	36	. 33	. 27	. 22	.21	. 19	.23	. 14	. 15	. 19	, 13 , 1	.20	.23	.24	.23	.23	. 24	. 22	. 22	. 13	. 19
7/r		0.10	60.	0.10 0.11	.07	80.0 0.08	$0.13 \\ 0.12$	0.28	.34	.46	28	4.40	.39	.21	.20	0.10	0.7	. 17	.09	12	. 05	.07	. J &	-0.135	
nd (dir)	308 317 320	\neg	7	200	\sim	2	~ ~	~ (2 5	\sim	~ -	4 ($\overline{}$	\rightarrow	ကစ	\sim	3	~	-	~	$\overline{}$	$\overline{}$	_	_	∩:
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Jate/Fime	23.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.	134-37	20-20/ 20-23		/03-10	708-11	7JB-1Z 7JB-1Z	708-13	/U8-13 /U8-13	708-14	/08-14 /03-15	/08-16	/08-16	/08-16	/08-17 /08-17	/US-18	8/08-13	8/08-19	8/08-20	/03-21	3/03-22	/08-22	/08-23	/03-53	08/00-0900

t (sia)	÷	•	n	± €	٦		17 *	13	15.	11	1.1	T.	10	* ~	*	* ~	* <i>'</i>	* '	* ~			5	.,	5	** 5	א	* _	* '?	k ~	* ∵)	* ~⊃	Ð	٠. ص	l o	J)
****	56	, 5 ×	ာ	٥.	٠.) (٠.)	0.531	4	<u>ب</u>	-7	-r	0.475	5.03	0.550	•	្	Ω• n ⇒Ω	•	U. 654	0.733	0.744	0.00	~	?	9.0.0	~	• • •	2	1%	11.	. 74	.72	. i.2	0.625	. i. 2	~
2 i (a)	320	310	360	300	340	350	370	380	400	310	320	340	320	29.0	760	270	300	3.19	300	4.01	310	33.1	345	35.1	320	340		-		٠.	<₹	4	340	Ċ	4
*:		-0,015		-0.037	-1), 1)2.1			-3, 002	-0,005	3	-3.01.6	-0.021	-d. u su	- n - n - n		-0, 043	- J. 04:0	-1.137	-3.042	1 i 0 * (-4.033	150-6-		-0.110	-1,047	-0.011	-:) • (: I J	-1.031	\sim	=	- j. 053	=		·	-0.051
4+ (عود/۱۱۰)		٠		•			•		0.137		•			•		0.302		٠	0.342	•	٠	•	J. 328	0.247	0.302	J. 350	•	0,342	~	.26	о С:	.22	0.218	. 20	. 20
./L	~:	~		-0.232	₹₩	\sim	-0.307	_	-0,333	-0.13	-0.239	-0.245	-0.173	-0.132	_	-0.155	-0,149	-0.1.63	-0.127	-9.113	?	Ξ.	4.0.0-C-	-3.124	-0.112	-0.033	-0.129	-0.151	-0,111	-0.235	-0.241	-0.245	7.		-0.301
nd (fir)	312	315	316	324	310	244	342	333	313	324	321	333	332	304	31.1	117	31.3	31.5 31.5	315	3.24	31.7	33.5	31.5	305	314	33.7	323		\$ 20	× 1.1	330	330	325	323	334
) (555/m)	6.3	6.4	7.2	4.0	5.1	₽•†	5.3	5.7	4.1	5.5	5.5	त. स.	ن. د.	7.3		λ. δ. β	5. Č	3.0	7 13	رن د .	3.1	, ,	3.7		막 : :	7.5	7.	~ °	0.7	7.1	•		6.2	•	
Jate/Fine	08/03-0035	08/03-0105	03/03-0135	03/09-0205	00/01-0235	03/02-0305	08/09-033a	J8/49-4443	08/33-3429	06/49-9505	03/39-0535	08/09-0603	u3/03-0530	03/39-3701	0.1/09-0730	0.0/0.9-0753	08/09-0630	03/03-0050	03/09-1125	06/05-1005	3/39-1019	0.5/0.5-1.033	0.5/42-1100	3/10-1142	36/03-1332	3./33-122.	0.0/0.9-1330	33/33-1353	06/39-1530	0.6/0.9−1530	03/39-1554	os/39-1700	08/09-173 0	3	08/09-133 0

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zi (a)	340 335	320	رنج منج د:	300	345	320	330	340	340	320	340	340	400	320	340	350	390	400	400	410	430	460	475	460	450	420	440	460	460	440	400	390	340
F.* (\$)			10.00.01 10.00.01	10.000		- 0. 056	-a.e.a.		-0.077	-0. Oak		. 0.	# 90°0-	19.03	-0.000		•		•	-0,132	•		-0.085		•	•		•			-0.059	-0.041	-0.033
)*(1/sec)	0.214		0.217	• -	-		٦.	7	0.215	ci.	\neg	~	-3	е.	0.074	7	_		. 2	S	. 2	. 2	. 1	7	٦.	7	Τ.	7	7	٦.	. 2	\sim	C:
z/r	2 +	-	~ ر~		। नो	-1,493	-0.377	-0.319	~	-0.275	-0.54g	:0	\sim		٦,	7,7	3	9	ব	~	~	. 2	4.	. 7	6.	.	•	-0.656	٠,	-0.463	-0.337	-0, 303	~d•226
ind) (dir)	335 338	S	יי חי	- ~	~	`~	\sim	$\vec{}$		$\overline{}$	٠,٣	\sim	~	$\overline{}$	_	\sim :	7	€.	\sim	\sim	\sim	C_1	\sim	~	_	~	~	7	7	c:		\sim	
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esta/cine	1-(0/	2/17-175	3/33-501	3/37-53 3/37-21	3/03-213	3/33-223	5/01-222	2/01-225	3/31-2	3/11-0	5/10-0	(-CIV)	(-01/c	5/13	3/13-3	1/1/-)	3/11-0	0/1.)-:)	3/13-03	3/13-99	3/13-19	ŭ∕10-1J	3/10-11	8/10-12	3/10-13	3/10-13	3/10-13	4/10-14	3/10-14	3/10-14	03/10-15.05	3/10-15	/1.)-1:

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(305/is)	. 6.1	بازر	0.532	٠. ت	.57	.42	36	. A J		. 05	<u>.</u> 5.	ن	.47	. 52	٦,	. 50	7		. U.	0.343	.35	. 36	.37	. 53	. 45	. 4 ú	.52	. 13	. 54	(T)	. 31		.33	0.455	٠٤,
2i (a)	300	260	240	300	290	230	200	250	300	230	200	180	110	140	200	270	140		. 🤈	200	-		S	~	₹**	3	S	\sim	=	S	3		200	330	200
т* (к)	-0.041	-0.040	-0.034			0.011		٠		-u. 022	-0.023						0.000					0.011	•	0.005	0,002			•		-0. 003		0.015	•	=	9.003
]* (m/sec)	.2	\sim	0.246	Ç	.2	\sim	٠,	~	~	٣.	٠,	٠,	٠,	~	~	7	. 2		. 2	.2	.2	. 2	7		. 2	\sim	\sim	٠,	2.	~	C:	\sim 1	\sim	.3	\sim
7/7	J. 2	ः	-0.162	7.	٦.	t	ે.	\Box	٦.	٦.	0	?	7	O	٦.			~		਼	С.	\neg	=	٦,	$\overline{}$	୍ଦ	$\overline{}$	$\overline{}$	-0.034	3	-0.062	୍	-0.047	-0.040	-1), 1) 0 2
nd (dir)		309	323	321	330	331	332	334	342	316	326	321	330	332	325	326	322	321	319	316	324	325	332	313	31,7	311	303	311	293	303	304	305	312	31 /	305
(n/sec)	٠ • •	•	7.0	•				•	•		•		٠	•	•	•		•	•	•	•	•	•	٠	•	•	•		•				•	٠	•
uate/rine	06/13-1034	3/13-1		3/10-1	3/10-2	3/1:1-2	3/11-2	3/13-3	3/10-3	ï	3/13-3	3/13-2	3/11-0	3/11- :]	111- 0	3/11-	7	=	03/11-0400	1	بآ	7-1	1	1-1	7-	1-1	1-1	1-10	1-19	1-50	111-51	3/11-23	3/11-22	/11-33	

t (ain)	C :0	10 8 8 11 10	17	7 7 13 *	* **	35 * 20 * 11 8
(Des/m)	0.349	0.350 0.383 0.382 0.413	28	0.272 0.281 0.253 0.328	33	-0.113 -0.255 -0.292 0.293
5i (a)	140	200 180 190 270 200	210	120 100 100 260		240 300 200 140
Τ.κ. (κ)	-0.001 0.002 0.005 0.005 0.003				0.029 0.029 0.029 0.020 0.004 0.034	
U* (m/sec)	22 17 12 11 12 14	24	69	20.00	0.154 0.154 0.137 0.139 0.139 0.168	233
3/17	5225		24 31 46 52	55.55	-0.519 -0.309 -0.140 -0.182 -0.250 -0.254 -0.053	000000000000000000000000000000000000000
nd (dir)	322 332 293 293 293 293	308 308 295 316	301 242 231 265	274 298 295 290 329	2310 2310 234 299 295 295	304 299 312 325
// (366/m)					ម្រាងឧយងឧម្មហ្ក នៃកំណុចប្រកប់ នៃកំណុចប្រកប់	
bats/rine	a/12-502 3/12-503 4/12-510 4/15-513 3/12-514	/12-023 /12-030 /12-033 /12-035 /12-043	/12-053 /12-053 /12-055 /12-063	/12-072 /12-074 /12-034 /12-083 /12-385	08/12-0940 03/12-1047 03/12-1047 08/12-1400 08/12-1500 08/12-1900 08/12-1900	8/12-193 8/12-203 8/12-213 8/12-215 8/12-230

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t (.ain)	()	* 0 2 2 2 3 3 4 5 1 6 6		DI D
(295/E.)	0.333	-0.261 -0.156 -0.156 -0.350 -0.387		0.408 0.383 0.377 0.413 0.433 0.557
%i (m)	120	300 230 200 280 300 310		240 200 200 250 260 240 210 200
Ψ*(X)	-0.013 -0.015 0.014 0.012 0.012	0.000000000000000000000000000000000000	0.000 0.000 0.000 0.000 0.000 0.000 0.019	0.013 0.013 0.013 0.017 0.015 0.015
U* (a/sec)			0.2897 0.3865 0.3865 0.3898 0.3898 0.499	
3/1	-0.161 -0.156 -0.246 -0.132 -0.120	-0.02 -0.002 -0.003 -0.003 -0.016 -0.072	- 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0	-0.023 -0.021 -0.020 -0.020 -0.021 -0.021 -0.039
nd (dir)	314 233 293 303	310 324 322 317 316 303	315 3115 3115 310 310 313 313 313	303 303 303 311 310 313 313
1i (m/sec)			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
Date/Fime	3/12-233 3/13-000 8/13-004 3/13-012 3/13-012	3/13-030 8/13-032 8/13-035 8/13-045 8/13-053 8/13-053		3/13-150 3/13-150 3/13-153 3/13-153 3/13-1/2 4/13-1/5 4/13-1/5
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w* (a/sec)	Ì	0.557	. 59	. 51	4.	.50	70	. 55		52	, 61	.71	.77	5.	.71	0.601	, 56	. 55	.46	44	. 53	3	. 48	. ŝ1	()	. 59	.53	. 4 ú	.47	. 4 C	. 45°	4.4	4.	. 45		3.3
2i (a)			$\overline{}$	\odot	\sim	\sim	ď	380	3	4	9	മ	20	\circ	20	2	\sim	4	3	マ	4	ಶ	_	\sim	- 7	10	•	\circ	\sim			∽	5	₹*	44	33
* (?)		. 01	. 01	. 02	.04	. 03	. J	0°008	. 03	.00	.01	60	. 04	• 05	. 07	11	.10	,11	.12	.13	. 14	. 15	ŝ	, 15	.15	.13	13	. 13	1.	. l.4	.15	2	70	-0.155	15	-0.033
(3/8ec)		45	49	.51	5.4	53	. 45	0.431	.41	.38	. 35	.36	.28	. 25	. 18	120	RO.	.07	.05	40.	80.	.07	. 07	. 08	7.	. 13	20.	. O	. 07	. 05	÷.	. 05		0.076	3	ריי
2/E		03	03	.02	01	7	.02	-J. U2403	. O.S	.07	,20	0.26	. 56	.31	3.51	. 03	99	2.88	.27	33	5.51	. 53	2.22	.33	.53	3.43	444	. U.	6.05	.17	.23	. რს	⊛	. 33
nû (dir)	. 1	311	312	310	310	310	310	300	310	315	326	330	332	330	35.7	312	300	309	319	329	40	76	100	1:14	151	137	160	₹	.5	5	ď	-	_	233	ó	3.10
ûni⊬) (Sec)		2	2.	ب	€ #	3	-	11.4	į.	÷	•	•	•		•	•					•				•	•	•	•		•	•	•	•	•	•	•
Date/Fime		3/13-132	1/13-194	3/13-233	3/13-210	3/13-212	3/13-225	03/13-2325	3/13-235	3/14-003	3/14-005	3/14-012	3/14-015	3/14-023	3/14-025	3/14-035	3/14-043	3/14-045	3/14-052	8/14-063	8/14-065	8/14-073	8/14-080	2	/14-035	/14-093	/14-100	3/14-102	011-61/0	/14-113	/14-120	/14-122	/14-133	/14-132	71	06/14-1436

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2i (m)	120	140	140	140	140	110	140	140	150	190	130	250	300	2.30	230	280	280	290	270	230	300	270	300	220	160	170	160	220	260	260	240	240	210	180	310
ř*(X)		-0.105		-0.120	-0.075		-0,038			0.010		_				-0.005	•	•			•	-0.017		€.	-0.016	-0.015	٠.	٦.	Ξ,	۲.	ં.	୍	÷.	€.	-0.023
U* (-a/sec)	•	0.170	•	•	•	•	0,352	•	•	0.231			•	•	•	•	•	٠		•			0.131	•	•	0.200	•		•	•	•	•	0.068	•	0.059
2/L	0	-33	~	<u>د</u>	4	_	_	-0.167	_	_	€.	1,7	~	•	د،	C1	Ci	د.	-		=	, -	₹;	-			-0.163	4	1,5	C.1	5	ر م	-3,532	0	4.
nd (dir)	~	_	_	Ci	CI	\sim	\sim	\sim	~``	C,	\sim	\sim	\sim	_	_	\circ	$\overline{}$	\sim	~	\odot	~	-	238	C	\sim	_	c_1	~		~	7	\sim	550	S	?
in (۳/sec)	4.5																		•								•			•	٠		1.9	•	•
Dats/rime	03/11-1153	7	ಃ∩	- آن -	7	-1	7		01/11-20,00			1	$\frac{1}{1}$		•		T.	'n	33/15-3132	i.	Ĭ,	'n	1/15-	į	5-1	5	3/15-1	5-0	<u>(i - 5</u>	3/15-17	1-17	5-03	J	7	03/15-0957

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3/L	-0.909	3.9	J.	. 99	. o7	. 50	.33	.70	.79	.53	. 69	.94	33	.36	.19	36.	96	23	40.	94	.05	55.	.13	.65	74	. 59	.44	. 34	20	.21	.21	4	-0.272
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(§) *2	-0, 321	-0, 023	-0.025	-0, 323	-0.037	-0.032	-0.020	0. 002	ú, 000	F(1:0 *(1-	0.003	0 . 635	-0. one	9. Cun)	-0.003	0.00	0,003	0.005	0.003	0.00)	•	d. 30:	0.011		0.633	0.021	-:J. dl.3	-0,003	-0.001	J. 605	-:), 01 l	-d. ada	_	/ Or . C-	-0.386
U* (a/sec)	0.225	~	0.247	0.436	•	0.253	0,283	0.279	•	0.342	•	0.352	J. 346	0.346		•	1, 398	0.443	0.443	0.455	0.146	٠		•		0.413	0,396	0.441		•	0.475	0.464		. ; !	0,336
7/r	_	-0.153	-0.143	$\overline{}$	-0.175	-0.221		-3,124	_	100.0-	-0.373			-0.347	-10.039	-0.037	-0.033	-0.125	-0.025	-0.022	-0.023	-0.022	-0.023	-0.023	-0.008	-0.017	-0.075	-0.653	-0.043		-0.051	-0.050	<u> </u>	-0.042	-0.073
ns (dir)	32 ů	121	327	(건 항	3.11	315	313	313	304	30.5	315	312	33.2	314	315	315	30)	312	312	396	312	315	303	31.2	313	31.2	311	311	315	320	(H	57	ب	317	324
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13/17-3130	10.0	327	-0.053	0.407	-0.005	360	0.720	*
15/11-0233	12.0	91.0	-0.019	0.460	-0.005	360	0.753) (3)
03/17-9233	7.1	324	-0.100	0,346	-0.016	360	0.720	*
13/17-1245	7.1	325	-0.139	0.263	-3,024	350	0.030	ر د
13/11-3333	7.9	317	-0.151	0.237	-0.026	360	0,703	*
13/11-0347	7.9	325	-0.166	0.285	-0.023	420	0.743	₩
14/17-3430	8.3	321	-0.096	0.298	-0.024	410	0.647	77
13/17-0451	7.6	317	-0.130	0.269	-0.031	460	0.672	11
09/11/-0800	8.1	319	-0.065	0.288	-0,003	510	0.581	15 *
18/17-0635	7.9	317	-0.076	0.279	-0.006	009	0.626	16 *
13/17-0705	5.7	322	-0.130	0.194	0,003	099	0,535	21 *
14/17-0735	3.8	349	-0.436	0.123	-0.010	540	0.508	21 *
14/11-3805	2.1	46	-2.099	0.071	-0.039	0.30	0.497	21
13/17-0335	2.3	24	-1.545	0.092	-0.054	520	0.561	* 27

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	Zi	(F)	240	240	200	220	240	240	260	260	350	310	290	210	210	210	290	290	330	330	330	350	380	340	540	540	540	540	540	540	430	430	460	450	460	600	600
	* č1	(y)	-0, 068	_	-0.038	-0.101		•	•					-0.067		٠	•		-0 . 035	٠		-0,035			٠	٠			-0, 0.35		-0.035	٠	-0.041	-0.053	-0.042	-0,033	-0.053
C ta	* 7	(m/sec)	0.140	, 13	\sim		, 14	15	. 13	<₹	. 10	. 15	15	.33	.27	. 24	.21	6T.	13	• 16	. 15	$^{\sim}$. 13	9	11.	Ŝ	. 04	. 11	. o.	.o.	. L3	≈	. 13	<u> </u>	. 2.2	<u>~</u>	. 21
	7/2		S	.52	, d1	-0.389	5	45	53	. 50	4 ≥	.41	4		.10	0.09	.11	12	. 14	٠١,	. 22	\sim	. 13	. 14	. J.	.19	, 28	-1.054	.07	. 62	-0,349		. 13	$\frac{2}{3}$		-0.336	\odot
	nd	: t	232	232	232	282	23.2	232	292	282	303	303	303	302	302	302	302	302	302	3J3	303	303	303	303	303	303	130	313	313	313	31.3	313	313	313	313	313	313
	i,	(m/sec)	•	•	•	3.7	•	•	•	•	•	•	•		•		•		•	٠			•	٠	•	•	٠	•	•	•	٠	•	•	•	٠	٠	•
	Jate/Pine		6/02-135	5/02-142	5/32-152	05/02-1559	/02-152	/02-105	32-172	102-175	3-095	103-102	703-105	13-115	/33-122	/03-125	13-112	/03-135	/33-142	/03-145	/03-152	/03-155	/03-175	03-132	/04-102	/34-102	/34-132	/14-11	/04-113	$\overline{}$	/04-133	6/34-140	5/114-114	/04-151	/04-154	5/04-132	704-135

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2i (n)	520 520	520 520	350	350	27.0	270	200	200	180	110	150	1.60	190	250	250	300	260	260	250	260	260	200	320	320	320	320	290	230	290	290	200	200
Ţ* (K)	-0.043 -0.030	-0.023	-0.090	-0,033	-0.0/0 -0.040	-0.051	$\overline{}$	-0.056	-0,324	-0.016	-0.018	-0.012	-0.007	-0.034	-0.016	-0.003	-0 . 005	-0.011	-0.010	0,014	0, 022	0.010	-0.043	-0.012	-0.044	-0.010	-0.005	-0.022	-0.007	-0.017	-0.038	600.0-
('a/sec)		7.7	0	G (= ~	• ~	•	<u>ب</u>	٦,	7	?	C.			7.	7	٦.	~	-	٦.	3	7		.2	~	. 2		٦.	4.	7.	7	?
7/7	-0.130	-0.100	-3,342	-2.644	•	-0,305	-0.295	-0.259	-0.104	-0.054	-0.053	-0.038	-0.076	-0.157	-0.107	-0.067	-0.037	-0.192	-0.133	•	0.143		•	•	•	•	-0.057	•	•	-0.169	•	-0.032
nd (dir)	313	230 290	300	303	303	303	303	303	303	302	302	302	303	303	303	303	303	303	31)3	363	303	303	303	303	3.12	302	302	303	301	301	273	273
ir (m/sec)	10 10 1		•	•	•		•	•			•		•	•	•	٠	•	•	•	•	•	٠	•	٠	•	•	٠	•	•	•	٠	•
Date/Time	0.4 - 1	/04-20 /04-20	705-09	(0-50)	07-50/ 07-50/	/u5-10 /u5-11	/U5-11	105-12	705-12	/05-13	705-13	705-14	1.15-16	705-16	705-17	11-50/	705-18	/05-19	705-19	735-20	705-20	105-50	702-10	735-11	/06-12	100-13	7.16-15	/06-15	106-16	06/06-1734	6/01-12	6/07-13

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ì	υatc/rime	Aind (m/sec) (ط	nd (dir)	7/7	U* (a/sec)	F* (X)	Zi (a)	(m/30C)	t (.ain)
	00/07-1352	6.7	273	-0.031	0.229		200	0.268	1.2
	00/07−1459	7.0	302	-0.133	0.243	-0.034	200	6.543	3
	u5/07-1526	0.0	303	-0.234	0.224	-0.030	200	0.537	
	05/07-1555	7.0	303	-0.117	0.211	-0.032	150	0.357	1
	05/01-1629	0.0	302	-0.021	0.222	0, 001	150	0.202	12
	0501-10/0	6.1	303	-0.423	0.204	a. vo2	150	0.183	13
	00/01-1757	4.0	302	-0.051	0.335	-0.027	150	0.427	· o
	06/01-1629	7.5	342	-0.017	0.259	0.012	150	0.205	1.2
	05/01-165)	9°0	302	-0.016	0.305	0.009	150	0.247	10
	02/1-10/00	S. 5	302	0.337	0.205	0.641	150		
	35/07-1753	7.2	\$02	\$ 50°0	0.234		15.0		
	00/01-2025	ن. د	303	900.0-	0.500	0.025	150		
	da/00-031	1. ₃	~	-0-46A	0.057	0.003	6.90	0.235	7)
	00/00-0844	2.0	~	-0.423	0,001	0.003	063	0.240	1.1
1	90/10-00/00	2.2	~;	-0.011	0.054	0.014	680	0.055	173
11	05/05-0521	1.0	7	-2.2.12	0.035	-0.007	080	0.263	<u>د</u> د
L	0.0/03-0344	1.3	₹	-1.710	0.045	-(), .)].1	080	0,302	30

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- 1. For a more complete description of the experimental equipment see: "Experimental Aspects of a Shipboard System used in Investigation of Overwater Turbulence and Profile Relationships," T. Houlihan, K.L. Davidson, C.W. Fairall and G.E. Schacher, NPS61-78-001.
- 2. The following reports give more complete descriptions of the cruises:

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